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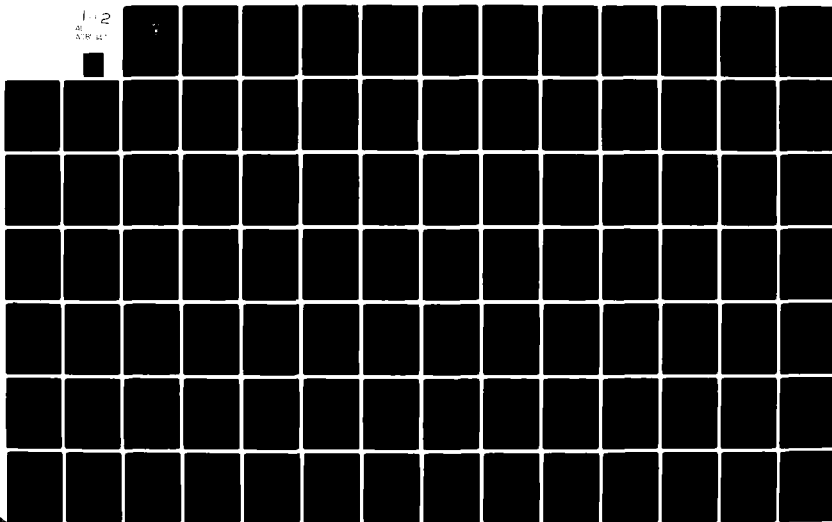
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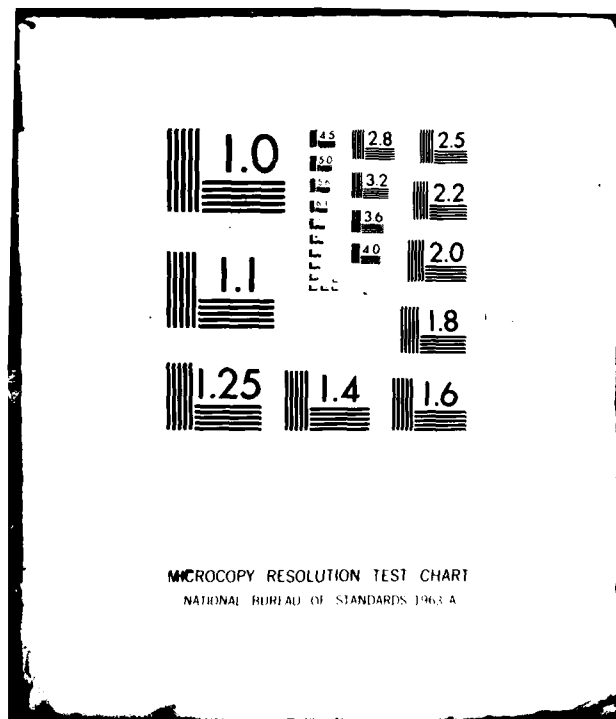
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GUIDANCE AND CONTROL OF TACTICAL MISSILES

by

Thomas Alan Grote

December 1979

Thesis Advisor:

D. J. Collins

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Guidance and Control of Tactical Missiles

by

Thomas Alan Grote
Lieutenant, United States Navy
B.S.A.E., United States Naval Academy, 1974

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN ENGINEERING SCIENCE

from

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ABSTRACT

This thesis discusses the conversion of the MOD6DF computer program for use on the IEM-360 computer at the Naval Postgraduate School. The functioning program was modified to investigate the impact miss distance for the Supersonic Tactical Missile. When the initial y-displacement error exceeded 1800 feet, the missile did not acquire the target. All errors smaller than this resulted in miss distances within 0.5 feet of the target. The midcourse guidance reference altitude was changed to reflect a sea-skimming missile. This simulation ran and impact was recorded. An attempt at adding random noise to the homing seeker was tried, but revealed that more information is required on this topic. The MOD6DF computer program was successfully converted and altered to run using the simplified ramjet model.

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TABLE OF SYMBOLS AND ABBREVIATIONS

The following is a list of the abbreviations and some of the more common fortran symbols used in the MOD6DF computer program. Each symbol is defined in two ways. The primary source of identification is by its COMMON(3415) location and the second is by its fortran symbol. The fortran symbol is not always a good identifier since it will change from subroutine to subroutine (i.e. W and WE both are used for missile weight).

A. ABBREVIATIONS

<u>Symbol</u>	<u>Definition</u>
TP	tangent plane axes
BA	body axes
SA	stability axes

B. FORTRAN SYMBOLS

<u>Symbol</u>	<u>Definition</u>
TXBA(073)	missile thrust in the x-direction in BA (lb)
TYBA(074)	missile thrust in the y-direction in BA (lb)
TZBA(075)	missile thrust in the z-direction in BA (lb)
W(086)	missile weight (lb)
S(110)	missile reference area (ft ²)
CA(111)	drag coefficient
CY(113)	side-force coefficient
CZ(115)	normal force coefficient
CBAR(116)	mean aerodynamic chord (ft)
CMQ(118)	damping in pitch coefficient
CNR(119)	damping in yaw coefficient

<u>Symbol</u>	<u>Definition</u>
CLP(120)	damping in roll coefficient
CM(121)	pitching moment coefficient
CN(122)	yawing moment coefficient
CL(123)	rolling moment coefficient
CGI(136)	center of gravity (ft)
A(201)	moment-of-inertia about missile roll axis (x-body axis) (slug-ft ²)
B(202)	moment-of-inertia about missile pitch axis (y-body axis) (slug-ft ²)
CC(203)	moment-of-inertia about missile yaw axis (z-body axis) (slug-ft ²)
TSA(208)	angle between SA and BA (rad)
P(212)	missile angular velocity about x-BA (rad/s)
Q(216)	missile angular velocity about y-BA (rad/s)
R(220)	missile angular velocity about z-BA (rad/s)
AG(282)	unit conversion lb-slug
VXTP(286)	missile velocity in x-TP (ft/s)
XTP(290)	missile displacement in x-TP (ft)
VYTP(294)	missile velocity in y-TP (ft/s)
YTP(298)	missile displacement in y-TP (ft)
VZTP(302)	missile velocity in z-TP (ft/s)
ZTP(306)	missile displacement in z-TP (ft)
GZRO(404)	constant set to zero for flat earth gravitational field and set to one for a spherical gravitational field
ER(405)	angular velocity of earth (rad/s)
ALPO(406)	angle between north and x-TP (rad)

<u>Symbol</u>	<u>Definition</u>
OLAMO(407)	latitude origin of tangent plane
HO(414)	distance tangent plane is from earth (ft)
GO(415)	gravitational acceleration (ft/s ²)
HREF(501)	reference altitude for midcourse guidance (ft)
RE(503)	earth's radius (ft)
H(507)	altitude normal to earth (ft)
AMACH(520)	missile Mach number
THET(521)	missile pitch angle, TP (rad)
PSI(522)	missile yaw angle, TP (rad)
PHI(523)	missile roll angle, TP (rad)
GAMMAV(527)	vertical flight path angle, TP (rad)
VEL(528)	magnitude of missile velocity (ft/s)
VAT(529)	missile velocity (ft/s)
TF(550)	program termination time (s)
VAH(561)	computed speed of sound (ft/s)
ALAT(576)	latitude of target position (deg)
AZ(578)	azimuth of target position (deg)
DYNP(581)	dynamic pressure (psi)
FLGRJ(606)	constant set to zero indicates run will use ENGINE subroutine and when set to one run will use RAMJET subroutine (simplified ramjet model)
T(932)	actual time (s)
T1(933)	boost engine ignition (s)
T2(934)	commence acceleration command mode (s)
T3(935)	boost engine burn-out/port cover blow-in (s)
T4(936)	start ramjet engine (cruise) (s)
T5(937)	commence heading and altitude guidance control (s)

<u>Symbol</u>	<u>Definition</u>
T6(938)	commence terminal dive (s)
T7(939)	commence terminal guidance - search (s)
T8(940)	commence terminal guidance - track (s)
DMAX(1740)	maximum fin deflection (rad)
CPP(2669)	time between printouts (s)
ROLLO(2901)	initial roll angle (rad)
PITCHO(2902)	initial pitch angle (rad)
YAWO(2903)	initial yaw angle (rad)
STEP(2905)	determines executive program flow after staging
DOC(2909)	defines number of times COMMON will be printed
HMIN(2911)	minimum integration step size
HMAX(2912)	maximum integration step size
DER(1)(2913)	integration step size (s)

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I. INTRODUCTION

Research was undertaken to convert the MOD6DF computer program received from NWC China Lake for use on the IBM-360 computer at the Naval Postgraduate School. Once a functioning program was obtained, initial displacement error versus impact miss distance was investigated for the supersonic tactical missile. Additionally, the midcourse guidance reference altitude was changed to reflect a sea-skimming scenario and this was examined for its effect on the terminal guidance problem. This report not only discusses the aforementioned topics, but also describes the missile mission requirements and the MOD6DF computer program.

II. MISSION REQUIREMENTS

The Supersonic Tactical Missile (STM) mission is divided into six phases (Ref. 1).

- * initial conditions
- * separation
- * boost
- * transition
- * cruise
- * terminal

These divisions are based on the missile aerodynamics. The initial condition phase establishes the starting conditions for each launch. This is done while the missile is still attached to the launch platform. The separation phase starts when the missile is launched. The missile falls for approximately five seconds until the boost engine ignites. This initiates the boost phase which continues until the missile achieves Mach two. As the missile passes through Mach one, plume effects are encountered which the aerodynamics account for. At the end of the boost phase, the port covers blow in. This initiates the transition phase. This phase is very short and allows the debris to be ejected from inlet ports. The cruise phase commences when the ramjet engine ignites. This engine propels the missile until target impact. The terminal phase of the flight begins when the missile is commanded to dive from the cruise altitude. This phase concludes when the flight is terminated at target impact.

The six STM mission phases require four phases of control. These control phases are:

- * separation
- * midcourse guidance
- * terminal dive
- * terminal guidance

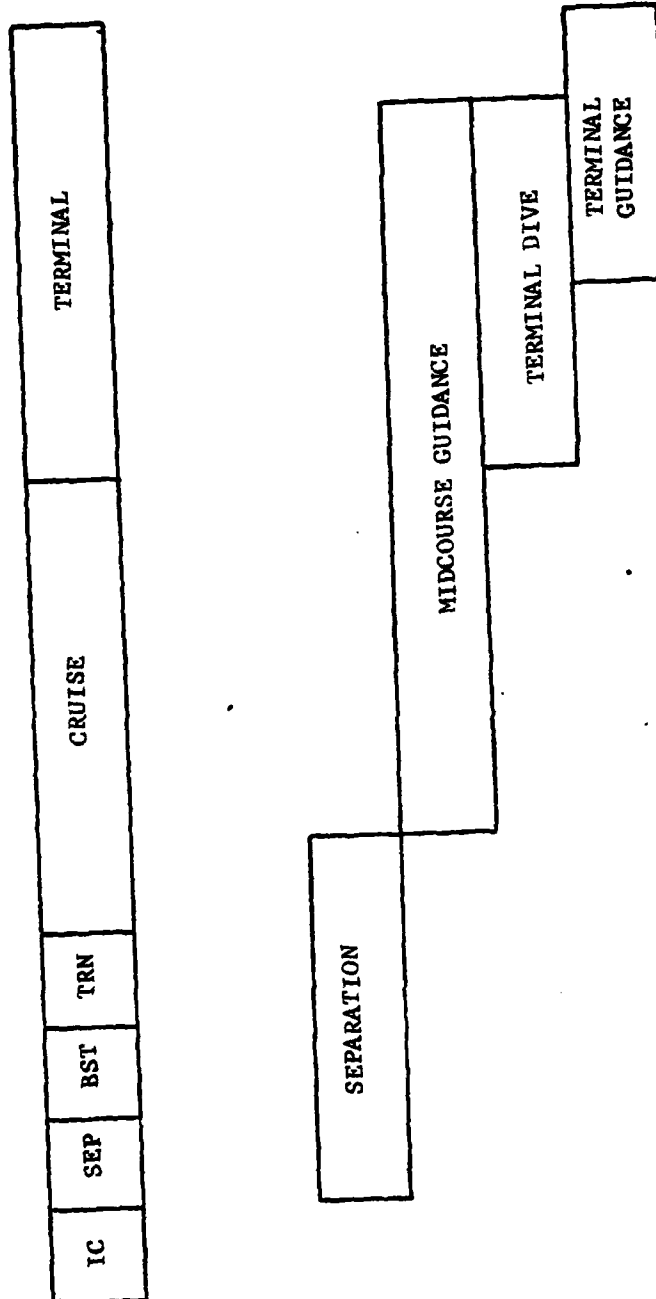
The four Guidance, Navigation, and Control (GN&C) system control phases are directly related to the mission phases. Figure 1 displays this relationship (Ref. 2). To obtain a successful flight, various types of control and guidance functions are required. Figure 2 (Ref. 3) illustrates the guidance control mode sequencing in relation to the mission phases and also indicates the critical missile switching times. The control phases are discussed below, along with the appropriate guidance modes.

A. SEPARATION

The separation phase commences upon launch. The missile is ejected downward from the launch platform. Additionally, the pitch attitude of the missile is commanded down. Since this portion of the flight is unguided, the ejection force and gravity are the only forces acting on the missile. At launch, the missile is required to be in the attitude command mode.

Five seconds into the flight, the missile pitch attitude is commanded up and the boost engine is ignited. The booster continues until the missile attains Mach two, at which time control is shifted from attitude to acceleration control mode. The acceleration control then requires the missile to maintain the normal and lateral accelerations at zero.

The last event to occur in the separation phase is inlet port cover blow-in. The time delay that allows the port covers to clear is a function of altitude.

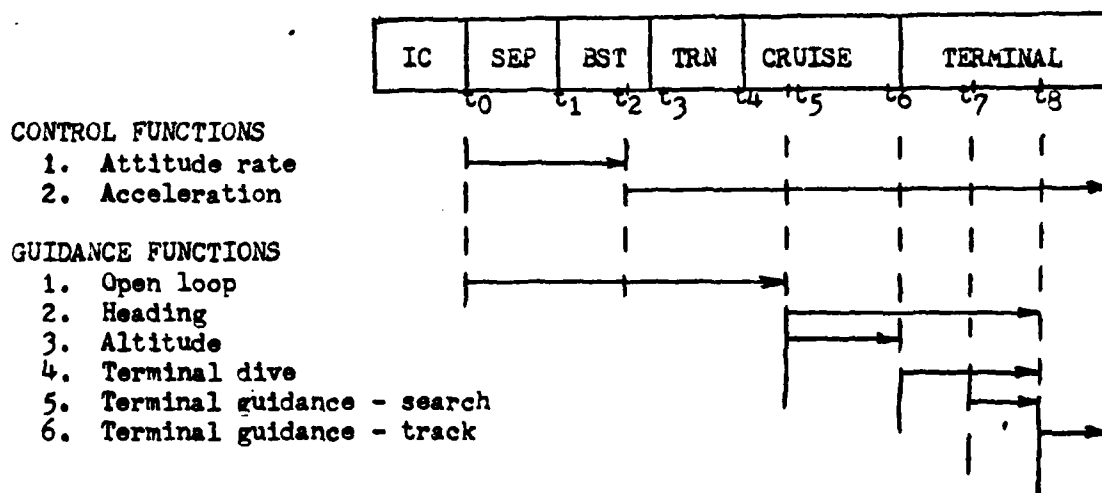


IC - INITIAL CONDITIONS
 SEP- SEPARATION
 BST- BOOST
 TRN- TRANSITION

CONTROL PHASES/MISSION PHASES
 RELATIONSHIP

FIGURE 1

- t₀ - LAUNCH: START SIMULATION
- t₁ - BOOSTER IGNITION
- t₂ - CONTROL SYSTEM MODE CHANGE FROM ATTITUDE TO ACCELERATION CONDITION AT M=2.0
- t₃ - PORT COVER BLOW-IN, BOOSTER BURNOUT
- t₄ - RAMJET IGNITION, t₃ + .3 sec
- t₅ - ENGAGE GUIDANCE MODES
- t₆ - DIVE COMMAND
- t₇ - SEEKER SEARCH MODE IS ACTIVATED
- t₈ - TERMINAL TRACKING



FLIGHT MODE SEQUENCING

FIGURE 2

B. MIDCOURSE GUIDANCE

Midcourse guidance begins upon completion of the separation phase. The moment the port covers are clear, the phases shift. During this phase two things are required. The GN&C must guide the missile to the established cruise altitude and then guide the missile (in the horizontal plane) to the predetermined target location.

To accomplish these requirements the GN&C system employs both altitude and heading control. The altitude control acts upon the pitch axis to drive the missile to the cruise altitude and then to maintain that altitude until the terminal dive phase commences.

The actual guidance work is performed by the yaw axis. The GN&C system uses the heading control to steer the missile to the target position. To generate the steering commands a guidance law is necessary. The guidance law should minimize the cross-track error and the final lateral acceleration. A minimum cross-track error allows for minimum flight time and minimum displacement error when target search is initiated. Minimizing the final lateral acceleration ensures that the seeker will continuously be pointing toward the target area. To insure accuracy, the guidance law must be able to perform these functions when subjected to disturbances such as wind and thrust misalignment.

C. TERMINAL DIVE

The terminal dive phase commences when the missile is commanded to dive. The actual time that this command is given is a function of the predetermined target coordinates. Upon diving, the missile must accelerate downward along a 60-degree (from horizontal) dive angle to the target position. Once the missile has steadied up in the proper dive aspect, terminal guidance commences.

D. TERMINAL GUIDANCE

During the terminal guidance phase the seeker is required to search, acquire, and track the target. The GN&C system then uses these tracking signals to direct the missile to the target. The seeker uses a preprogrammed search pattern to locate the target. When the target has been acquired, the seeker then commences tracking it and also notifies the GN&C system that the target is being tracked.

Target acquisition takes place when the target falls within the instantaneous four-degree beamwidth pattern as it traverses the scan pattern on the earth's surface. The computer program uses this assumption since the exact missile target acquisition mechanism has not yet been defined.

Upon acquisition, the GN&C system closes the seeker tracking loop. The radiometer error signal is defined as the difference between the look vector and the line-of-sight. This signal is used to reposition the antenna gimbals so the look vector and the line-of-sight coincide. Under the closed loop operation the radiometer output is proportional to the line-of-sight rate and this is the signal used to guide the missile to target impact.

III. COMPUTER SIMULATION

The modularized six-degree-of-freedom (MOD6DF) computer program was developed by the Litton Systems, Inc., Guidance and Control Systems Division (Ref. 4) to be used in analyzing missile guidance and control. The program uses a building block approach, where each module corresponds either to a missile subsystem or an environmental system. In its original form, the program is used primarily for terminal guidance of air-to-surface missiles. The Naval Weapons Center, China Lake modified the original program to specifically apply to the Supersonic Tactical Missile (STM). The modification also allows the user the capability of simulating any portion of the missile flight trajectory.

The MOD6DF computer program consists of four main decks and one auxiliary deck. The main decks include the executive programs, operational subroutines, modules, and input data deck. All the subprograms utilized in the integration and the sequencing of the modules are contained in the executive programs. The operational subroutines are used by the user to control the program while it is running. The physical system and the environmental subroutines are included in the modules. The input data deck contains all the information the executive programs need to execute the desired run. Lastly, the auxiliary deck consists of all those subprograms (subroutines and functions) that are required by the modules.

Once the user starts making simulations, he must concern himself with program sequencing. Proper sequencing is required to ensure a valid run is achieved. Since it is of such importance, sequencing will be discussed as the final part of this section.

A. EXECUTIVE PROGRAMS

The executive programs are the main core of the MOD6DF program. These subroutines have various functions in setting up, sequencing, integrating, and resetting the program. Since these functions are required by any type of analysis done, the user should never have to change any of these subroutines. Reference 5 should be consulted if the user desires more information about the content of any of the subroutines described herein.

1. Zero

Subroutine ZERO is used to set all the COMMON(3415) locations to the value zero. This is done to ensure that no erroneous information is used in the simulation.

2. Oinpt1

Subroutine OINPT1 is the basic input routine for the MOD6DF program. The normal input is from punched cards. However, inputs may also be read from tapes. The basic input cards will be discussed in the section covering the input data deck.

3. Auxi

Subroutine AUXI is used to call the initialization modules for each run. Additionally, it sets up the list of state variables which are used in AMRK.

4. Auxsub

Subroutine AUXSUB is used to call the dynamic modules. In calling the dynamic modules, AUXSUB sets and resets the lists needed for AMRK and the COMMON(3415) storage cells with the most recent values of the state variables and their derivatives.

5. Amrk

Subroutine AMRK is the integration subroutine. It uses a point-wise first order Runge-Kutta method. All the state variables to be integrated must be listed in COMMON(3415) and also must appear in a processing list.

6. Reset

Subroutine RESET is used to reinitialize up to fifty input parameters. This is done prior to the start of any repeated runs. To indicate which parameters are to be reset, the number one is punched in columns 46-60 on the respective type three card.

7. Return Group

The return group is a collection of all the unused modules. Since all the modules and their initialization modules are called by AUXI and AUXSUB, the unused ones must still remain in the deck. These are required to ensure proper linking when the computer attempts to link all the subroutines. All the subroutines in this grouping contain three cards. The three cards are the subroutine title, and a return and an end card.

8. Sub11, Sub12, Sub13

These subroutines are used to call the operational subroutines that are required. They call the routines in the order prescribed by the input data deck. The number at the end of each subroutine title indicates which operational subroutines it can call. For example, SUB11 can call STGE1.

B. OPERATIONAL SUBROUTINES

The operational subroutines provide the user with control of the program while it is running. The order in which the operational subroutines are called is specified by the input data deck. Since these routines assist the user in controlling the simulation, they can be reprogrammed. However, it is advised that they not be changed until the user has become quite familiar with the overall operation and sequencing of the MOD6DF program. For more in depth knowledge of the operational subroutines the user should consult Ref. 6, and the computer listing, which is contained at the end of this report.

1. Inpt1, Inpt2, Inpt3

These subroutines are available for new inputs during the simulated flight. The only one presently used in the program is INPT1. It is utilized to input a namelist file which is used by ENGINE and is described there.

2. Oupt1, Oupt2, Oupt3

These subroutines allow for the print-out of up to fifty different variables during the flight simulation. OUPT1 is not utilized in the deck. OUPT2 is used when the desired output is to be put on tape. OUPT3 is the basic output routine. It prints the desired output on regular computer paper.

3. Stge1, Stge2, Stge3

These subroutines allow for proper staging, run termination, etc.. Presently STGE1 is not being used. STGE2 is being used as the staging initialization subroutine. STGE3 is the primary subroutine of this group. It stages when impact with the earth is made, when the final time, TF(550), is reached, or when LCONV(2672) is set equal to two. All the tolerances for staging are listed in STGE3.

4. Cntr1, Cntr2, Cntr3

These subroutines allow the external dynamic control inputs to the modules. In the MOD6DF program these are not used.

5. Rndm1, Rndm2, Rndm3

These subroutines allow random noise to be added to the state variables generated in the modules. RNDM1 is not used in the program. RNDM2 is used as the initialization subroutine, while RNDM3 provides continuous noise values. These subroutines produce correlated noise values for as many modules as required. The noise values remain fixed during each individual integration cycle.

6. Auxa1, Auxa2, Auxa3 Auxb1, Auxb2, Auxb3 Auxc1, Auxc2, Auxc3

These subroutines are auxiliary routines that allow for external input, output, control, etc. of the modules. At the present time, none are utilized in the MOD6DF program.

C. MODULES

The modules are of prime importance to the user since they represent the 'model' of the dynamic system. In general, the model is described by ordinary non-linear time-varying differential equations with both random and deterministic forcing functions. The user must first reduce these equations to an equivalent system of first order equations, which can then be described by each module. Generally speaking, the physical system is so complex that this would be impossible to do. However, due to the modularity of the MOD6DF program, the user can think of each module as a completely independent system described by the equations within that module.

There are thirty-six possible modules divided into five functional

categories. Each group is identified by a letter which pertains to that group's function; A (airframe), C (computers), D (dynamics), G (geophysical), S (sensors). A complete printing of each module is contained in the computer program listing.

1. Airframe

a. Subroutine A1

This is the aerodynamic forces and moments module. It calculates all the necessary forces and moments in body axes. These values are then used in the computation of the dynamics.

b. Subroutine A2

This is the missile aerodynamic coefficient module. It calculates the required coefficients using the information stored in the BLOCK DATA. Using the timing inputs, this routine computes the coefficients for the different effects. Some of the effects accounted for are; plume, separation, and control surfaces effectiveness. With this done the total coefficients are determined.

c. Subroutine A3

This is the missile propulsion module. The timing inputs are used to determine whether the missile is in free fall, boost, transition, or cruise phase. With this determined the correct engine subroutine (BOOST, RAMJET, ENGINE) can be called. Three variables are calculated using the body axes as the frame of reference. They are the missile thrust in all coordinate directions, the principal moments of inertia, and the missile weight.

d. Subroutine A4

This is the fin actuator module. The four control surfaces commands are calculated as either ideal actuators or as second-order

ones. In addition to control surfaces commands, the rate of change of yaw, and roll are computed.

e. Subroutine A5

This module is part of the return group.

2. Computers

a. Subroutine C1

This is the autopilot module for the STV-G. It uses the cruise engine ignition time to divide the routine into boost/separation and cruise phases. These two phases use different algorithms to calculate the turning moments in pitch/yaw and roll.

b. Subroutine C2

This is the guidance command module. Using the timing inputs, this routine is divided into separation/boost, dive/climb, cruise, terminal dive, and terminal homing sections. Each section uses slightly different algorithms to calculate the guidance commands to maintain the proper flight profile.

c. Subroutines C3 - C10

These modules are part of the return group.

3. Dynamics

a. Subroutine D1

This is the translational dynamics module. It computes the total acceleration in body axes and then converts them to the tangent plane reference. Then, accounting for aerodynamics, thrust, gravity, and coriolis, the velocity and acceleration are calculated.

b. Subroutine D2

This is the rotational dynamics module. With the principal axes as a reference, this subroutine computes the body angular rates and the attitude direction cosines.

c. Subroutines D3 - D5

These modules are part of the return group.

4. Geophysical

a. Subroutine G1

This is the gravitational and coriolis acceleration module.

It calculates the gravitational acceleration using one of two fields.

The user specifies the field to be used by an input card. To use a flat-earth gravitational field, GZRO(404) must equal 0.0, and to use a spherical gravitational field, GZRO(404) must equal 1.0.

b. Subroutine G2

This module is part of the return group.

c. Subroutine G3

This is the air data module. It computes the velocity, in all three coordinate directions, with respect to the air mass. These values are then resolved into body and stability axes. This module also computes all the properties of air by calling subroutine AIR. These values are stored in their COMMON(3415) locations for use in the other modules.

d. Subroutine G4

This module is part of the return group.

e. Subroutine G5

This is the coordinate conversion module. It takes the missile position, does a coordinate conversion and then it determines the position, velocity, and acceleration in the ECI system.

f. Subroutine G6

This module is part of the return group.

5. Sensors

a. Subroutine S1

This is the homing seeker module. It simulates the missile seeker and computes the seeker dynamics and Euler angle rates. Several flags are used to control the seeker sequencing:

- (1) FLAGS(335). FLAGS signals the start of the seeker search.
- (2) FLGT(317). FLGT signals when the seeker is locked-on.
- (3) FLGTS(347). FLGTS signals the end of search.
- (4) FLGD(336). FLGD signals when the seeker has detected the target.
- (5) FLAGLT. FLAGLT signals when the target is outside the seeker field of vision.

b. Subroutine S2

This is the radiometer module. It takes the target position and the ATIGS target position and converts them from body axes to the seeker axes. Using target position, the module then calculates the azimuth and elevation error signals.

c. Subroutines S3, S4

These modules are part of the return group.

d. Subroutine S5

This is the accelerometers and gyros modules. The user has the option of using ideal or digital accelerometers. To specify the type of accelerometer, the user must include the appropriate data statement in the subroutine. If ideal accelerometers are desired, FLGA must equal 0.0 and for digital accelerometers, FLGA must equal 1.0.

e. Subroutines S6 - S10

These modules are part of the return group.

D. INPUT DATA DECK

The input data deck provides the user with the means of specifying which operational subroutines and modules are to be utilized for the desired run. It also allows the user to set the starting conditions. In general, only the constants and the state variables must be given initial values. All quantities in COMMON not given initial values will be set to zero by ZERO. In addition to the state variables, the upper and lower error bounds must be initialized. There are seven types of input cards, each indicating a certain function.

<u>Type</u>	<u>Function</u>
0	read/write tape
1	operational subroutine to be called
2	module to be called
3	numerical input
4	printed output
5	parameter square and sum
6	termination and random noise generator input

A separate card is required for each subroutine, module, input, and output quantity. A sample computer printout of the input data deck is contained in the computer output section.

1. Type 0 Card

Type 0 cards are used to indicate if the type 3 inputs are to be read from or written onto an auxiliary tape. These procedures can be used rather than reading the inputs from a deck of cards. A typical card is defined by punching a zero in column 2. The field that covers columns 5 - 20 is used by the user for any descriptive statements with which he wishes to identify the input. Column 21 - 25 contains the right-

justified integer number of the tape transport to be used. The number of the first record to be read is punched in column 31 - 45. The last field is column 46 - 60 which contains the number of records to be read. The last two fields may use either fixed or floating-point notation.

2. Type 1 Card

Type 1 cards are used to specify which operational subroutines are called during the flight simulation. This type card is identified by the number one in column 2. The second field is column 5 - 20 which contains any identifying information. This information is printed out when the data deck is read and allows the user to read exactly which subroutines were called. Column 21 - 25 contains the right-justified integer number which is the subroutine identifying number. The operational subroutine numbers are;

<u>Subroutine</u>	<u>Subroutine Number</u>
INPT1, INPT2, INPT3	2
OUPT1, OUPT2, OUPT3	3
STGE1, STGE2, STGE3	4
CNTR1, CNTR2, CNTR3	5
RNDM1, RNDM2, RNDM3	6
AUXA1, AUXA2, AUXA3	7
AUXB1, AUXB2, AUXB3	8
AUXC1, AUXC2, AUXC3	9

It should be noted that all or any of the subroutines listed under one number can be called by including only one card. The cards are placed in the data deck in the order in which they will be called. This order or sequencing will be explained further in section F, Sequencing. A typical type 2 card is identified by the number two in

column 2. In general, column 5 - 20 should contain the module title, but any pertinent information is allowed. The module number is punched in column 21 - 25 and it must be right-justified. A listing of the module numbers follows:

<u>Module</u>	<u>Module Number</u>	<u>Module</u>	<u>Module Number</u>
A1,A1I	2	D4,D4I	20
A2,A2I	3	D5,D5I	21
A3,A3I	4	G1,G1I	22
A4,A4I	5	G2,G2I	23
A5,A5I	6	G3,G3I	24
C1,C1I	7	G4,G4I	25
C2,C2I	8	G5,G5I	26
C3,C3I	9	G6,G6I	27
C4,C4I	10	S1,S1I	28
C5,C5I	11	S2,S2I	29
C6,C6I	12	S3,S3I	30
C7,C7I	13	S4,S4I	31
C8,C8I	14	S5,S5I	32
C9,C9I	15	S6,S6I	33
C10,C10I	16	S7,S7I	34
D1,D1I	17	S8,S8I	35
D2,D2I	18	S9,S9I	36
D3,D3I	19	S10,S10I	37

Note that either the module, the initialization module, or both may be called by including only one card in the deck. A sample of a typical type 2 card is shown in Figure 3 (Ref. 7).

4. Type 3 Card

Type 3 cards are used to set any COMMON(3415) location to any value other than zero. In general, four items must be initialized. The state variable initial values and any constants used in the flight simulation are the most obvious. Additionally, there are some constants associated with the executive programs and operational subroutines and the state variable upper and lower bounds which must be initialized. As with all cards, column 2 defines the type card and it must contain a three. Column 5 - 20 holds the statement describing the input. The user should be specific here since it will save him having to remember every COMMON(3415) location. The only other means of input identification is by column 21 - 25. These columns contain the right-justified COMMON location of the input. Columns 31 - 45 hold the actual numerical value of the input. The last field, column 46 - 60, contains the reset flag. If the reset flag equals one, the COMMON(3415) location and the numerical value are placed in the reset list. This list may contain up to fifty different variables. This, in the case of multiple runs, allows the variables to be reset to its initial value prior to each run without additional input cards. The sample card in Figure 4 (Ref. 8) shows that either fixed or floating-point notation may be used to input the numerical value and the reset flag. These cards need not be inputted in any specific order, but for ease of checkout, it is advised to place them sequentially by their COMMON location.

5. Type 4 Card

The MOD6DF program can printout a maximum of fifty variables for each simulation. Type 4 cards are used to specify which variables are to be printed. Column 2 must contain the number four to indicate a type

4 card. When the results are printed out headings are included. These headings are designated in column 9 - 20. The exact alphanumeric title punched will be printed at the top of each page, this need not be the fortran symbol used within the program. The COMMON(3415) location of the output variable is contained in column 21 - 25 and must be right-justified.

6. Type 5 Card

Type 5 cards are used to indicate which variables are to be root-mean-squared. These cards are similar to type 1 and type 2 cards. Column 2 must contain the number five. Any pertinent information about the variable to be operated on is punched in column 5 - 20. The COMMON(3415) location of the variable must be right-justified in columns 21 - 25. The last field, column 31 - 45, indicates whether the root-mean-square operation will occur along the trajectory or at the end.

7. Type 6 Card

The type 6 card has two purposes. Its first function is trivial, but required. The number six is typed in column 2 and the rest is blank. This indicates to the computer program that there are no more input cards. Its second function involves random inputs. This card is used to indicate the number of random process (noise) generator cards that are to be read before the input process is terminated. Column 2 has the same information as before. Any pertinent information is contained in column 5 - 20. Columns 21 - 25 must be right-justified and they contain the number of random generator cards to be read.

E. AUXILIARY DECK

The auxiliary deck is a collection of subroutines and functions required by the modules. These routines are general in nature since

they can be called by several modules. They are used to calculate such things as the properties of air, engine performance, various ratios, and to locate values in the many data tables. A brief discussion of the most common subroutines is presented.

1. Boost

This subroutine calculates the thrust coefficient (CT) and the fuel flow rate (FF) during the boost phase. These values are returned to module A3 and used to calculate the missile thrust in the body axes and the missile weight.

2. Ramjet

This subroutine is used during the midcourse, cruise, phase of the missile flight. It uses a simplified ramjet model to calculate the thrust coefficient and fuel flow rate. This routine is not automatically called. The user must designate that he wishes to use it by inputting a type 3 card setting FLGRJ(606) equal to one. This then sets up the proper stepping in module A3.

3. Engine

This is the primary routine during the cruise phase. It is one of many routines within the NWC air-breathing propulsion package. This entire package is utilized to calculate the engine parameters from inlet to exhaust. Again, thrust coefficient and fuel flow rate are eventually computed and returned to module A3. The user does not need to supply any special input cards to use this subroutine. If no initial value is inputted for FLGRJ(606) it is automatically set to zero, which indicates this routine is to be used.

4. Air

All the properties associated with the air are calculated in

this subroutine. This includes the computation of the speed of sound and the dynamic pressure. Since the missile does vary in altitude, the routine takes this into account as well as the latitude. Once these values are calculated, they are returned to module G3.

5. Block Data

This routine contains data tables. These tables cover parameters from aerodynamic coefficients to thermal properties. The total data package covers specific bands within the missile operating envelope. Data is stored in matrices which includes one, two, and three dimensional ones. These data tables are readily available and there are routines designed to retrieve this information quickly.

6. Serch

This subroutine, along with several functions, is used to retrieve information from BLOCK DATA. If the present operating point of the missile is not within one of the bands of information, then the tables are interpolated. The functions THREDL, STDLI, STDLIA, and TAB do the interpolation of the tables. Since the tables are of various lengths, these functions are very general.

F. SEQUENCING

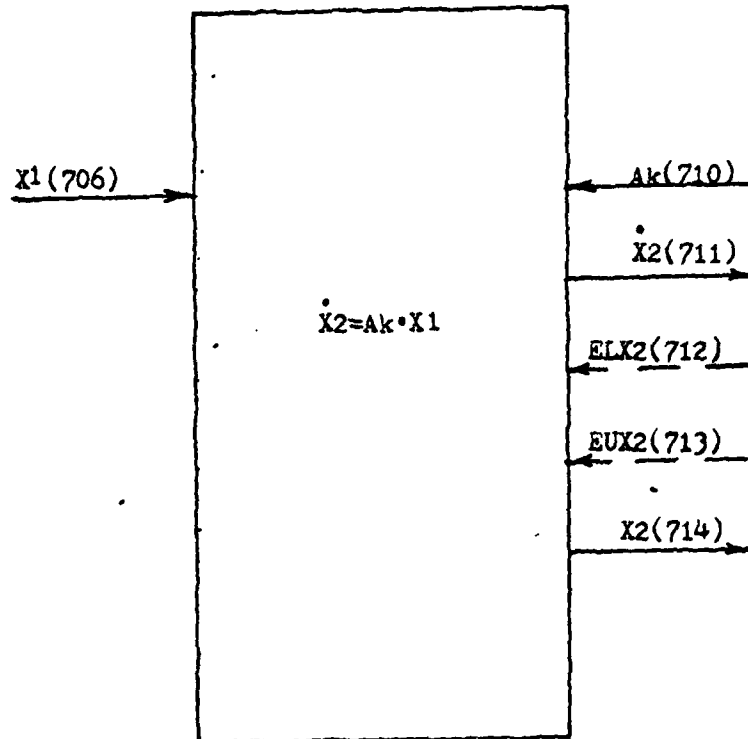
Sequencing is very important in the running of the MOD6DF program. Care must be taken to ensure that the modules are processed in the correct order at each step. This is essential to eliminate the use of obsolete values from the last cycle. An exception to this problem is the state variables. These are updated simultaneously by the integration algorithm. Any module is capable of using the most current value of these, no matter what the order of processing.

To help remedy this problem, module diagrams were devised. Module

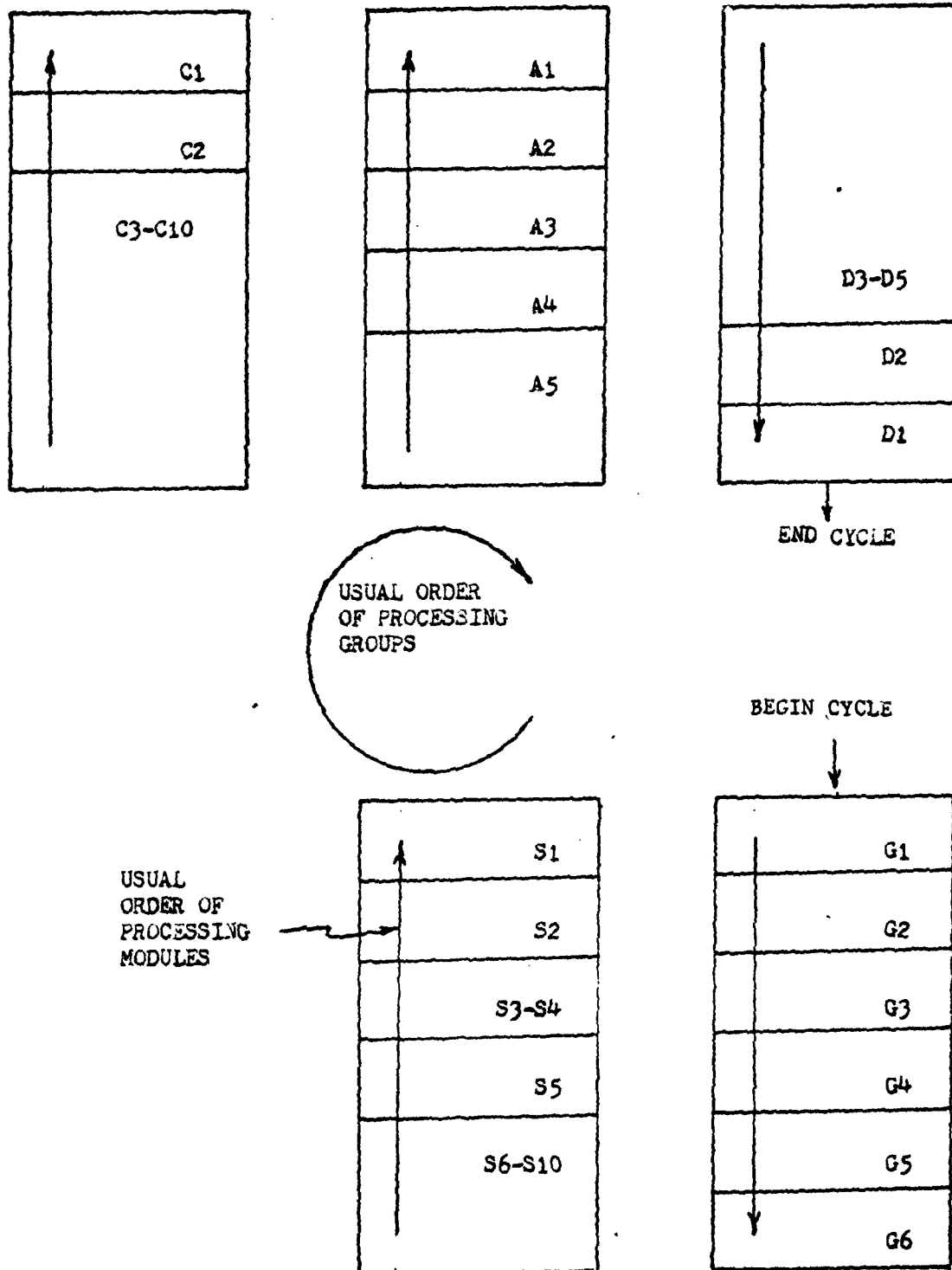
diagrams aid the user in maintaining the proper flow of variables into and out of the modules. To design a module diagram start with a box. This box will contain all the equations for a specific module. The standard procedure for showing inputs and outputs is to use arrows pointing in or out from either the left or the right side. The example in Figure 5 (Ref. 9) shows this technique. The arrows pointing in from the left indicate variable inputs from other modules. Arrows pointing out to the right indicate output going to either other modules or program output. The last set of arrows points in from the right. These show the constants brought in directly or indirectly from the initialization module. Since each arrow represents a variable, they must be defined. The usual means of labeling the arrows is to use the variable fortran symbol and in parenthesis its COMMON(3415) location.

Each variable usually has only one COMMON location associated with it. In the case of 'state' variables this is not true. State variables are defined by four consecutive COMMON locations. The first is for the derivative of the variable. The second and the third locations hold the lower and upper bounds, respectively, of the integration error. The last one contains the variable itself.

Once all the required module diagrams have been completed, they can be combined to get the overall processing order. The usual processing order, shown in Figure 6 (Ref. 10) is to start with the geophysical group, then proceed to sensors, computers, airframe, and finally dynamics. Within each group is a usual processing order and this too is shown in Figure 6. This process for determining the program sequence will eliminate the use of any obsolete values in the computer run.



MODULE DIAGRAM
FIGURE 5



PROCESSING SEQUENCE

FIGURE 6

IV. COMPUTER PROGRAM CHECKOUT

The basis for the research was the MOD6DF computer program from NWC China Lake. The total package received from them consisted of a listing of the program and an uninterpreted deck of cards. The initial step was to input the cards in small groups into the computer and then to examine the source listing. This listing revealed that the original deck was punched in BCD. This fact was easy to determine since several characters were changed (Ref. 11). The library routine NEWDEK was used to translate the cards from BCD to EBCDIC.

Once the translation was completed, an attempt was made to compile the new deck. This produced an output which contained many syntax errors. These errors were divided into two major groups. One effected the use of quotation marks in FORMAT and comment statements. The other one, the more difficult, effected the DATA statements in the BLOCK DATA subroutine.

The problem with the DATA statements was due primarily to the difference in the compilers used. The compiler at NWC was much newer and allowed for the use of more sophisticated inputs. The compiler at NPS only allows a data set to start with the first element. This required the rewriting of many data groups. To complicate these revisions, a limit of nineteen continuation cards is also imposed. These restrictions demanded not only the rewriting of many data sets, but also the formation of two new ones.

With the corrections finally completed, the computer would then compile the program. The next step was to link all the subroutines together. The first attempt was unsuccessful. Inadvertently, the subroutine INTR20 had been omitted from the original deck. Using the program listing, the contents of INTR20 were typed and included in the

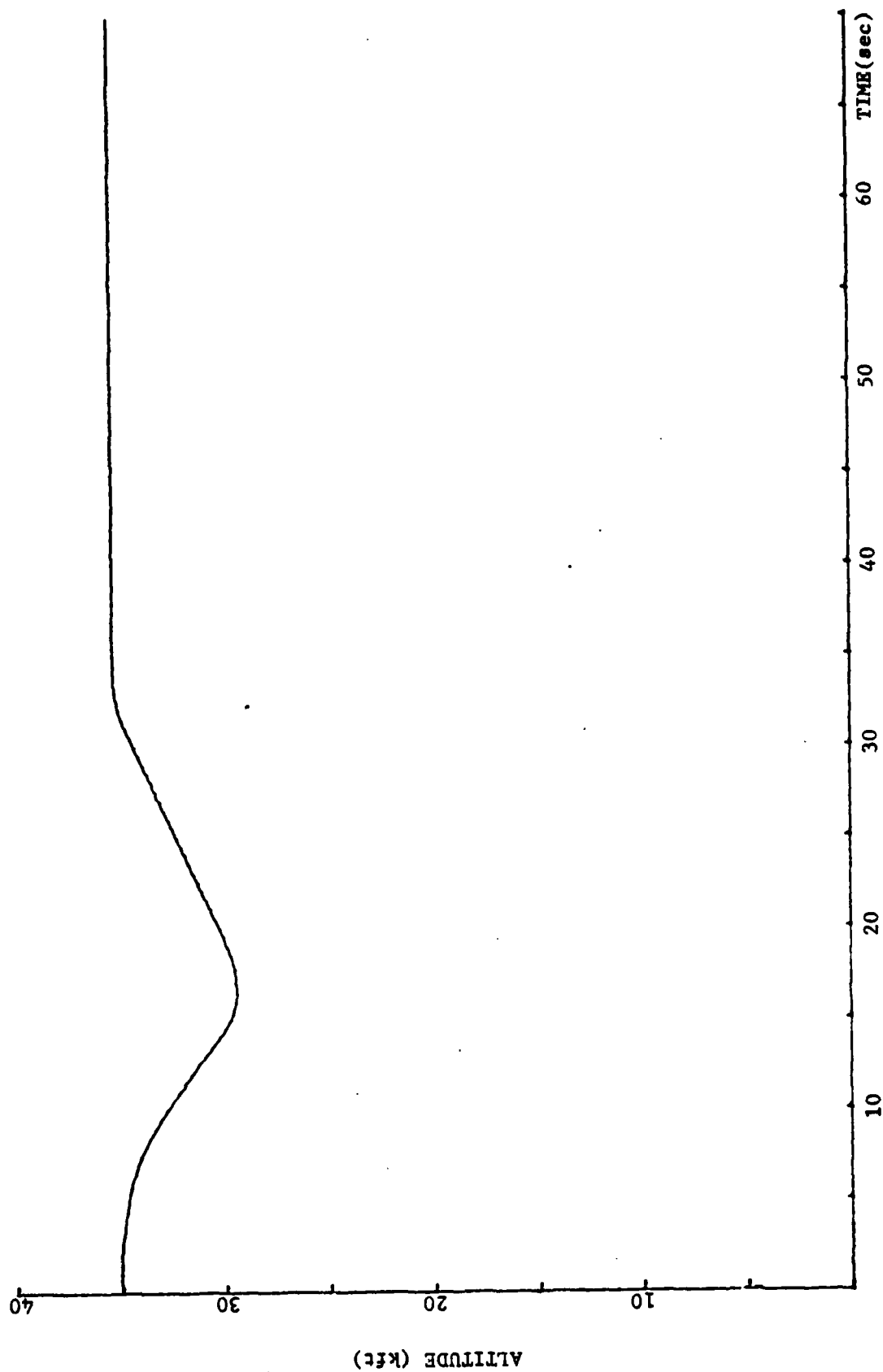
main deck. With this addition the program would now compile and link.

Now that the program would compile and link, attention was turned to getting a good simulation. To facilitate this process, two sample outputs were obtained from NWC. These outputs cover one missile flight which is broken down into a midcourse guidance and a terminal guidance simulation. Hereafter these will be referred to as midcourse baseline and terminal baseline, respectively. Using the initial conditions from the baseline models, it was hoped that the outputs could be duplicated.

A. MIDCOURSE GUIDANCE FLIGHT

The initial run, using the midcourse baseline inputs, revealed an overflow problem with the dynamic pressure (QD(508)). Using the traceback procedures outlined in the Users Manual from the W. R. Church Computer Center, the problem was confined to subroutine AIR. The problem turned out to be a translation error. The symbol $P\emptyset$ (\emptyset - zero) had translated to $P\emptyset$ in one place and P0 in another. This error caused the program to use a value left in that memory location from a previous run to calculate the dynamic pressure. With this problem remedied, the program could progress a little farther. The next stumbling block appeared as a divide check. These errors were resolved by introducing patches that would bypass a statement that tried to divide by zero. Once bypassed, that quantity would be set equal to zero. This was the normal procedure of the computer, but it would stop the run after ten such errors. Having corrected all these errors, output was obtained which covered the desired seventy seconds of flight.

When the output was examined a major switching problem within subroutine A3 (missile propulsion module) was found. The midcourse baseline utilized a simplified ramjet model, but the output was not.



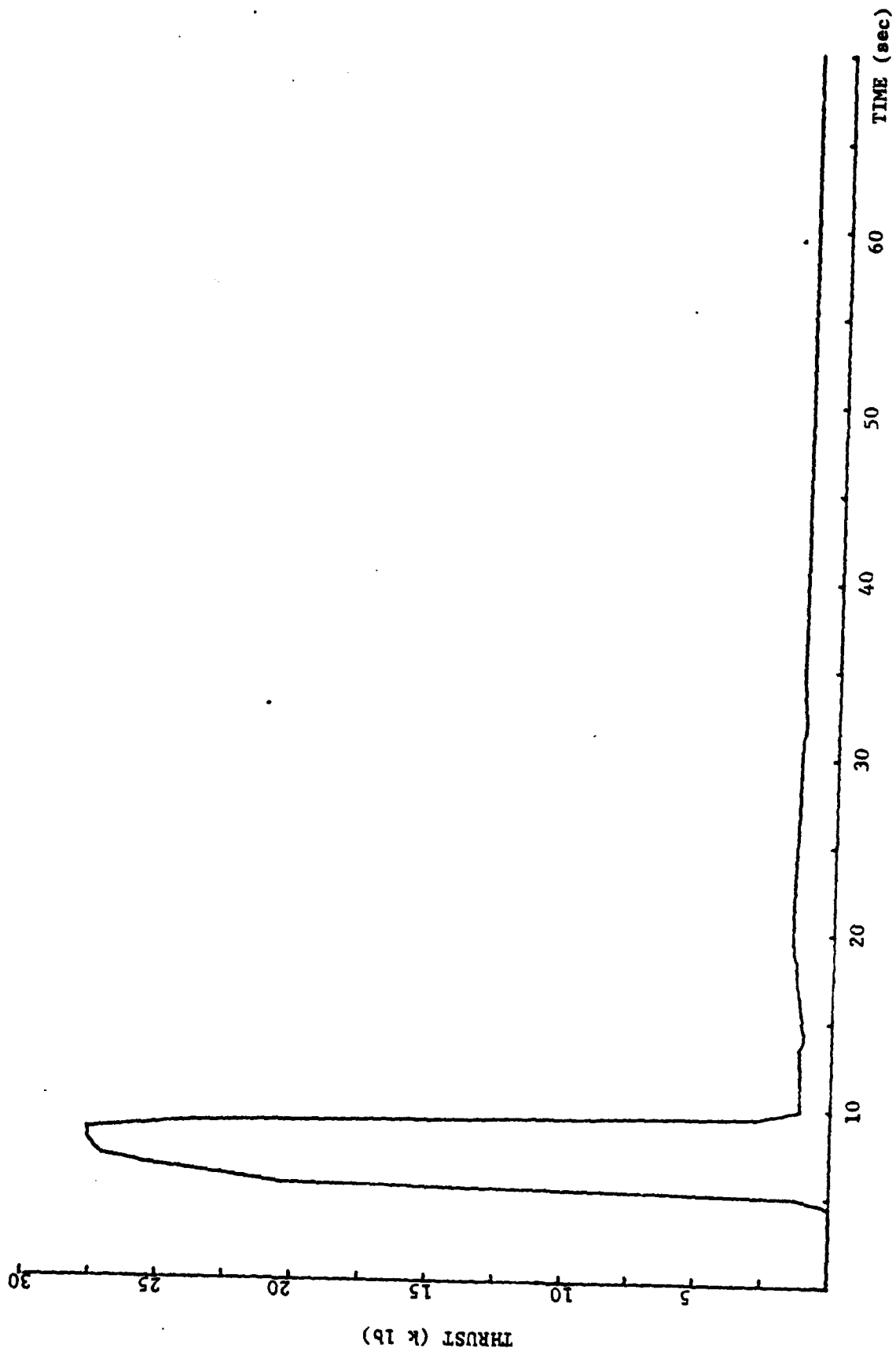
ALTITUDE VS. TIME (MIDCOURSE)

FIGURE 7

Rather than use RAMJET, the output disclosed that ENGINE had been used. The problem was in the logic statement, FLGRJ 0.0. The program was not making the desired switch to the simplified ramjet model. To remedy the problem, the data card FLGRJ(606) 1.0, was added to the input data deck. Another problem was discovered which occurred between 14.0 and 14.5 seconds. During that time period the missile angle of attack (ALPHA (330)) exceeded ten degrees. When ALPHA exceeds this angle the engine is turned off. With the engine off, no thrust is produced causing the forward velocity (VXTP(286)) to decrease. This limitation was removed from the program. After eliminating these problems a flight trajectory, Figure 7, was obtained which closely resembled the output of the mid-course baseline. A random sampling of the outputed variables were compared for exactness. The differences noted were due primarily to computer round-off error.

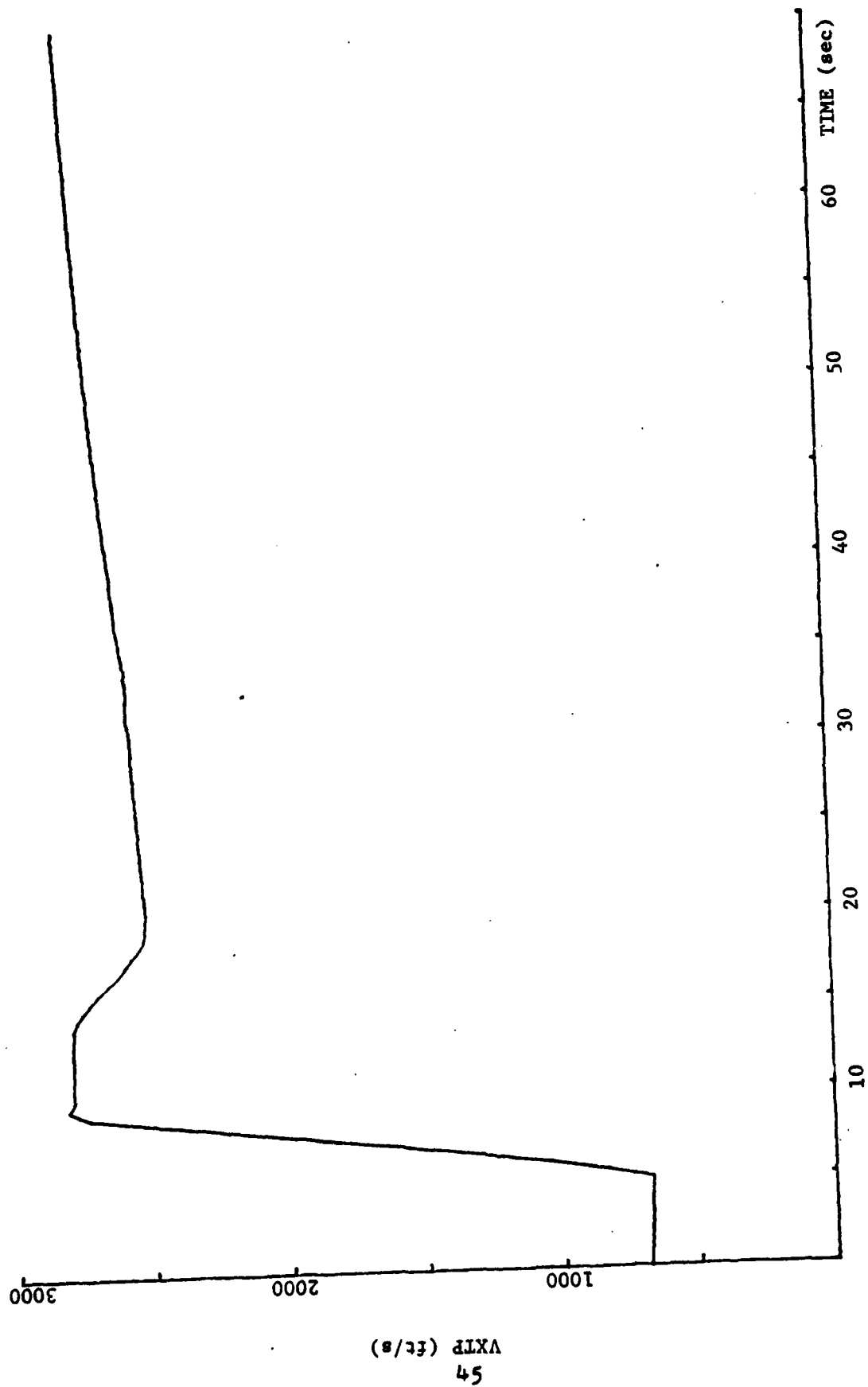
To further verify the accuracy of the two simulations, three parameter (TXBA(073), VXTP(286), and YTP(298)) were chosen as representative values for the runs. To obtain a feel for the run, these parameters are plotted in Figures 8, 9, 10. Additionally, random time samples are tabulated in Tables I, II, III.

The thrust (TXBA(073)) plot, Figure 8, can easily be divided into four mission phases. During the separation phase (0.0 - 4.5 seconds) the thrust is zero. This is expected since neither of the engines have ignited. This is followed by a rapid increase in the thrust. The maximum thrust, 27800 lbs, happens during the boost phase (4.5 - 9.5 seconds). At 9.5 seconds the boost motor stops and the transition phase occurs for the next 0.3 seconds. During this time the thrust decreases rapidly since neither engine is on. Once the engine port covers are



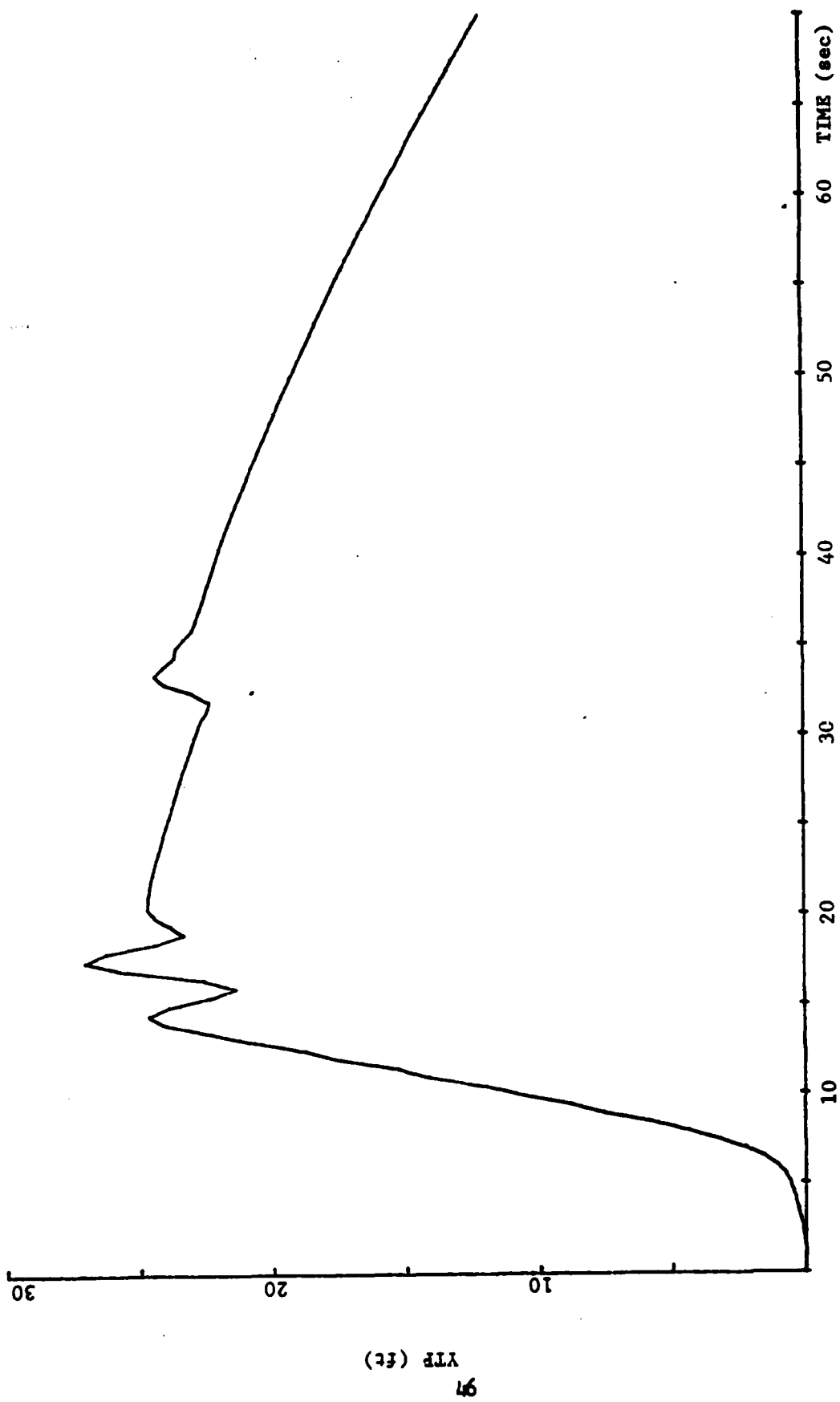
THRUST VS. TIME (MIDCOURSE)

FIGURE 8



VXTP VS. TIME (MIDCOURSE)

FIGURE 9



YTP VS. TIME (MIDCOURSE)

FIGURE 10

clear, the ramjet sustainer ignites. This action initiates the midcourse phase (9.8 - 70 seconds) and the thrust remains relatively constant at 1200 lbs.

The missile forward velocity (VXTP(286)) can be directly related to the thrust. During separation no thrust is produced, therefore the velocity is zero. As the missile is boosted to Mach two, the velocity increases and approaches its maximum value (2800 ft/s) just prior to boost engine shut-down. As the sustainer engine port covers clear, the velocity decreases slightly. Once the ramjet engine ignites the velocity profile is displayed in Figure 9 and it closely resembles that for the midcourse baseline.

The last parameter, y-displacement (YTP(298)), was included to demonstrate the accuracy of the guidance system. Figure 10 shows that prior to attaining the cruise altitude, the missile wanders off track. Once the guidance system is activated, it makes the necessary corrections to return the missile to the planned flight path. Table III shows that the y-displacement corresponds to the baseline case and at the conclusion of the run the off-track error is down to 12.03 feet.

All the information obtained from the new run was checked against the midcourse baseline. The results showed that the two simulations are within acceptable limits. With this milestone completed, the program checkout could proceed to the terminal guidance flight.

B. TERMINAL GUIDANCE FLIGHT

To checkout the terminal guidance portion of the MOD6DF program, the initial conditions from the terminal baseline were used. This required changing about a dozen input cards in the midcourse input data deck. The first run attempted turned out successful. This was due to the

TIME	0.0	7.5	10.0	20.0	25.5	30.0	40.0	50.0	60.0	70.0
BASELINE	0.0	27395	1140.6	1403.0	1377.4	1281.0	1211.3	1178.0	1148.1	1124.8
NEW	0.0	27391	1138.9	1514.3	1418.4	1314.3	1249.9	1207.0	1175.5	1149.7

TXBA (073) COMPARISON (MIDCOURSE)

TABLE I

TIME	0.0	7.5	10.0	20.0	25.0	30.0	40.0	50.0	60.0	70.0
BASELINE	681.99	1858.3	2790.2	2606.7	2604.9	2613.4	2652.4	2705.0	2743.8	2771.5
NEW	681.99	1851.7	2786.3	2506.4	2525.9	2544.5	2605.0	2665.5	2710.8	2743.9

VXTP (286) COMPARISON (MIDCOURSE)

TABLE II

TIME	0.0	7.5	10.0	20.0	25.0	30.0	40.0	50.0	60.0	70.0
BASELINE	-5E-5	3.46	11.37	27.21	25.92	24.34	20.45	16.93	13.24	9.39
NEW	-5E-5	3.19	10.68	24.43	23.93	22.82	21.96	19.14	15.81	12.03

YTP (298) COMPARISON (MIDCOURSE)

TABLE III

TIME	0	5.0	10.0	12.6	15.0	17.6	20.0	22.6	25.0	TF
BASELINE	1141.9	1131.0	1077.8	1170.9	1309.4	1501.1	1730.0	2245.3	2565.8	2691.3
NEW	1141.6	1134.8	1099.4	1212.8	1359.3	1561.7	1800.0	2305.9	2584.3	3273.6

TXBA (073) COMPARISON (TERMINAL)

TABLE IV

TIME	0.0	5.0	10.0	12.6	15.0	17.6	20.0	22.6	25.0	TF
BASELINE	2750.0	2764.2	2654.6	2471.4	2225.7	1854.5	1391.4	1376.9	1413.1	1425.0
NEW	2750.0	2761.5	2631.5	2438.7	2192.1	1828.2	1389.3	1366.7	1406.1	1465.2

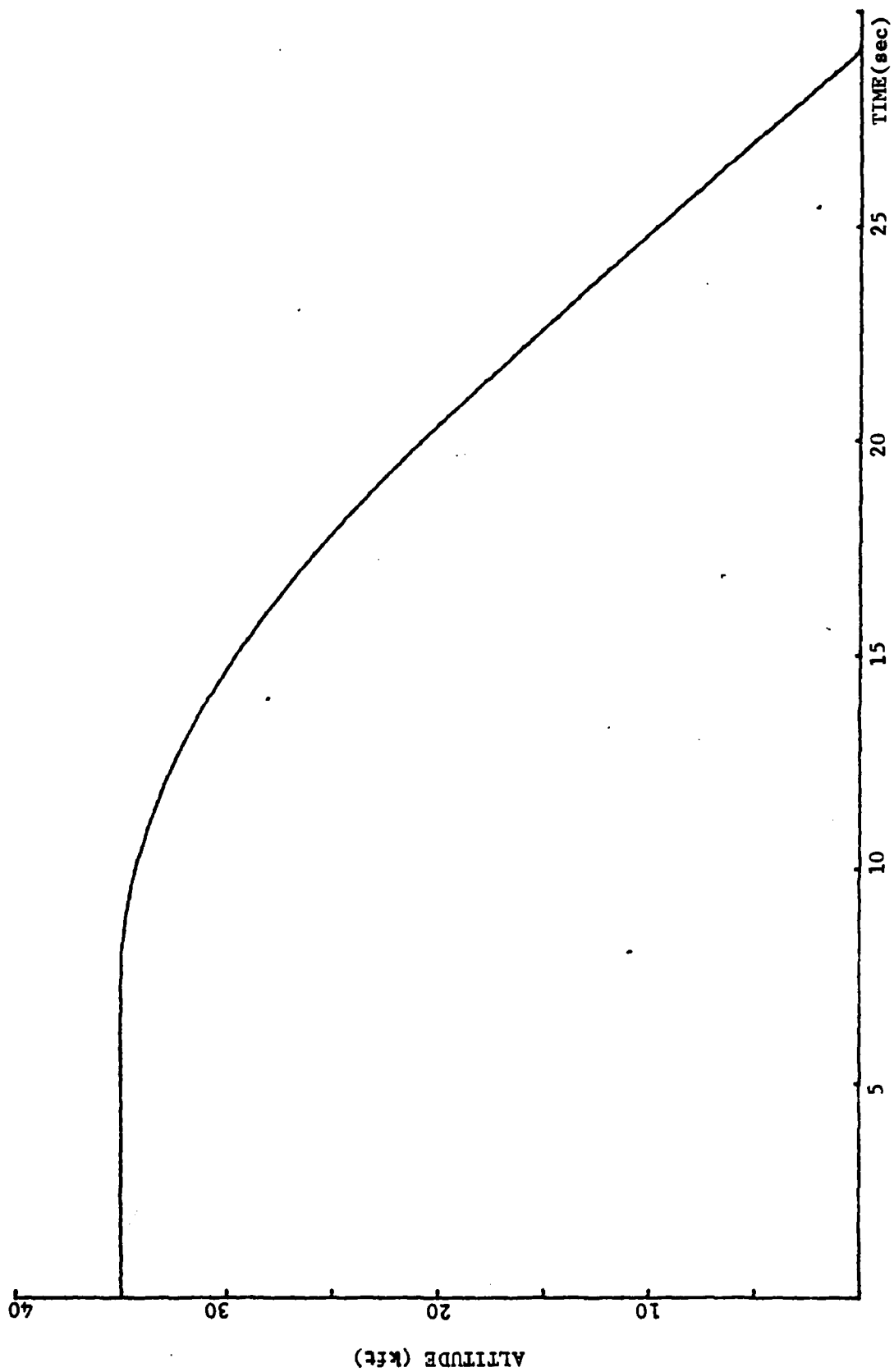
VXTP (286) COMPARISON (TERMINAL)

TABLE V

TIME	0.0	5.0	10.0	12.6	15.0	17.6	20.0	22.6	25.0	TF
BASELINE	0.0	0.0	$\sim 4E-6$	$\sim 5E-6$	$.7E-6$	$.9E-6$	$.1E-5$	$.2E-6$	$.1E-6$	$.1E-6$
NEW	0.0	$\sim .0074$	$.019$	-1.38	$-.095$	$-.868$	-1.77	$.071$	$-.151$	$-.05$

YTP (298) COMPARISON (TERMINAL)

TAVLE VI



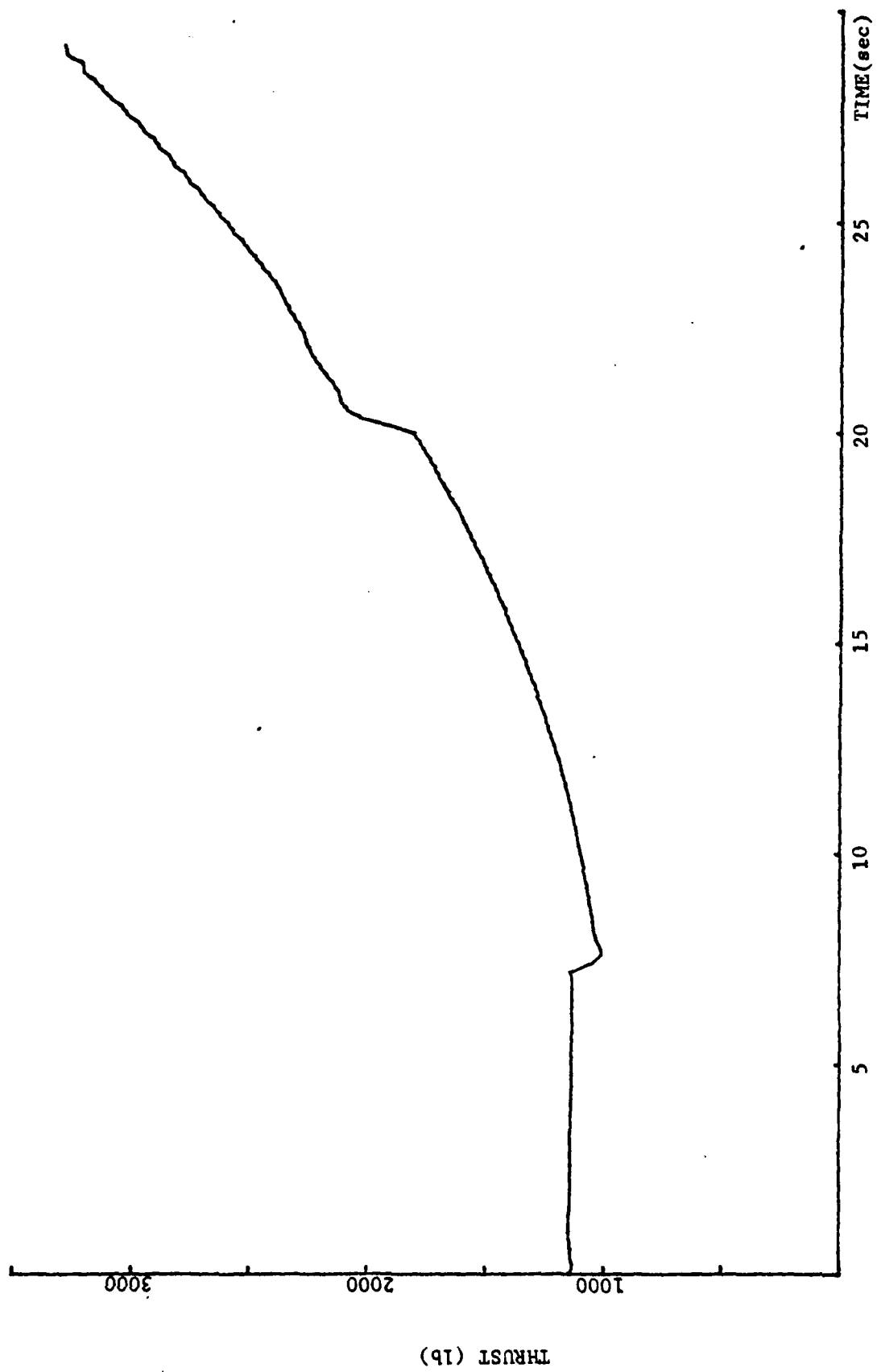
ALTITUDE VS. TIME (TERMINAL)

FIGURE 11

elimination of all the errors during the midcourse checkout. The resulting flight trajectory, Figure 11, is a very good illustration of the desired profile. To check the accuracy of the simulation, the same three parameters were chosen. Tables IV and V show that this run is almost identical to the terminal baseline. The difference is primarily due to computer round-off error. Figures 12 and 13 show the overall flight performance of the thrust and forward velocity, respectively.

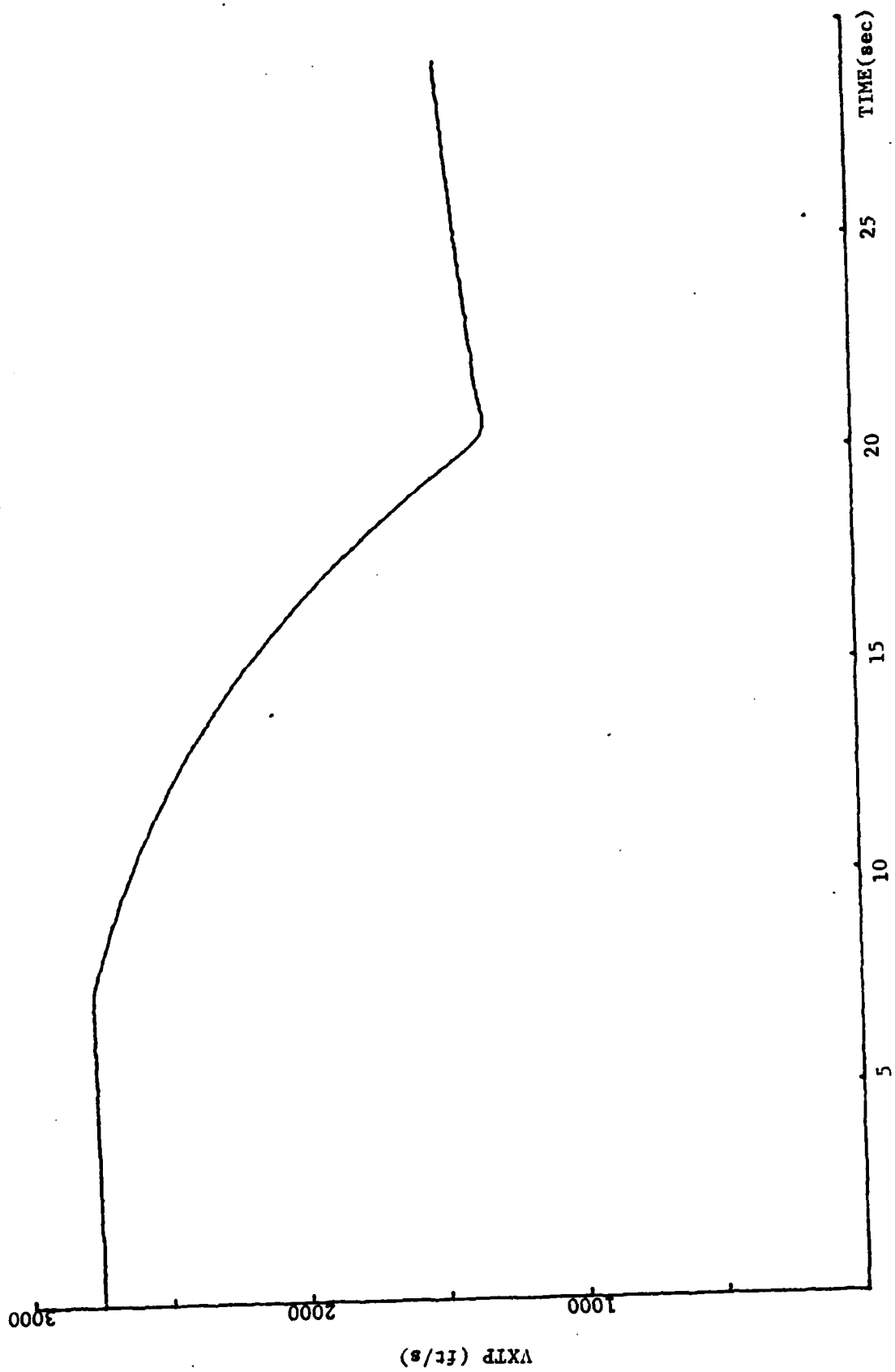
For this simulation, the y-displacement (YTP(298)) does not compare favorably with the terminal baseline. Figure 14 shows that between ten and twenty seconds in the flight, YTP develops rapid oscillations. By examining Table VI, it is noted that during this interval the two simulations differ the most. No reason for this discrepancy could be found. These oscillations do effect the flight by increasing the time of flight from 25.825 to 29.09 seconds and by increasing the miss distance. The imposed time constraints force this problem to be overlooked and to direct attention to the accuracy of the impact. Since the impact is within 0.5 feet of the target location, it is concluded that the terminal guidance simulation works properly.

With both segments of the MOD6DF computer program working correctly, thoughts could now turn towards the actual experimental runs. The results of these runs are discussed in the next section.



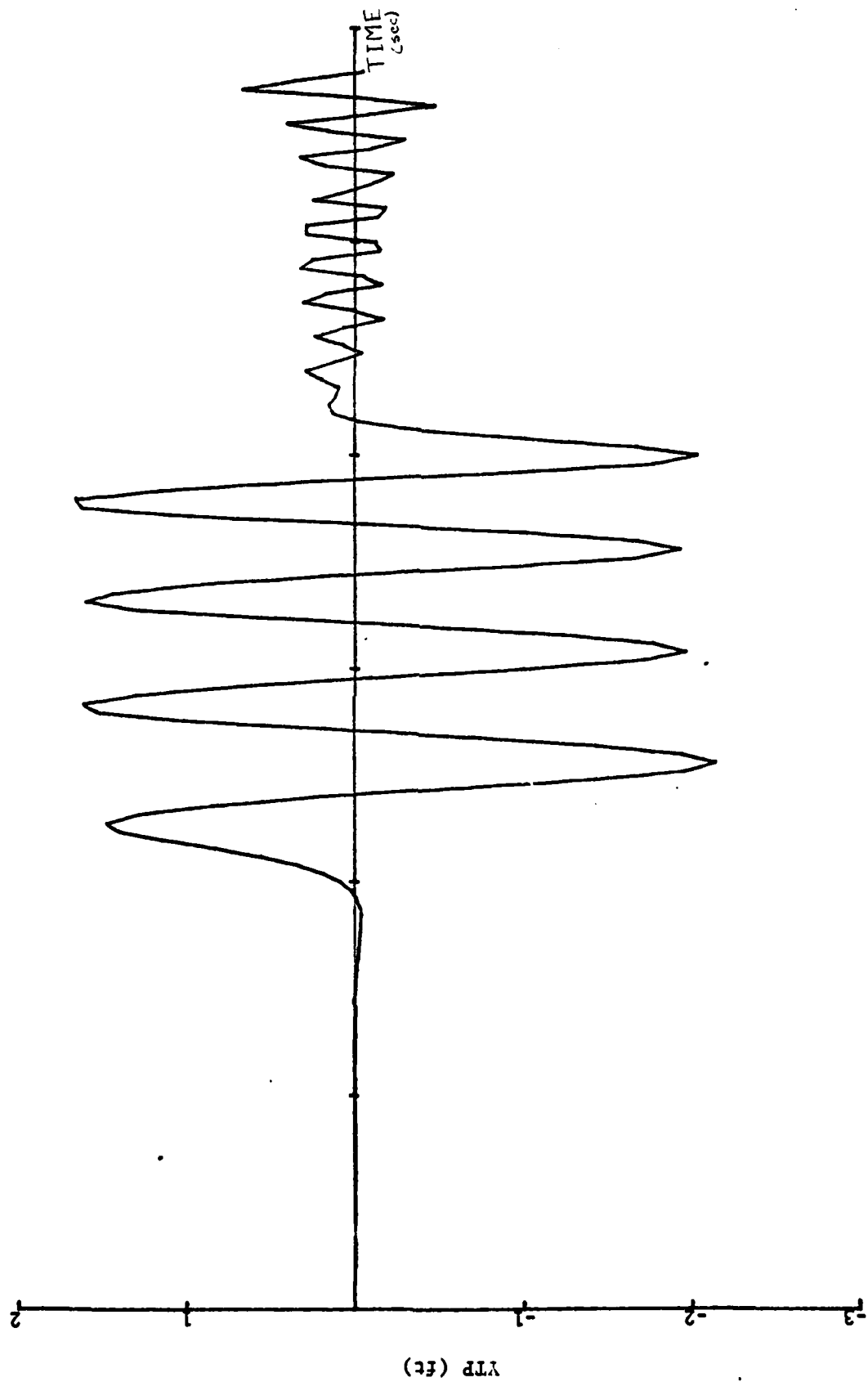
THRUST VS. TIME (TERMINAL)

FIGURE 12



VXTP VS. TIME (TERMINAL)

FIGURE 13



YTP VS. TIME (TERMINAL)

FIGURE 14

V. TERMINAL FLIGHT DISTURBANCES

With the checkout of the MOD6DF computer program completed, many ideas were discussed concerning alterations to the simulations. The three modifications decided upon were:

- * examine target miss distance when changes were made to the initial x-y-z conditions,
- * examine the terminal flight profile, range, and miss distance when the cruise altitude was reduced to approximate a sea skimming mode,
- * examine target miss distance when random noise is applied to the missile homing seeker.

To understand the changes and results, one must be familiar with the frame of reference. The origin of the reference frame travels from the launch platform to the target location at the cruise altitude. This is called the tangent plane reference system. Displacements in the x-direction (XTP(290)) are measured from the launch platform in the direction of the target. Y-displacements (YTP(298)) are measured left or right of the ideal flight path, in the tangent plane. Any vertical displacement (ZTP(306)) is measured normal to the ideal flight path, with down being the positive direction. Using this frame of reference the information in Table VII is easier to understand.

The first modifications demonstrate the effect of changing YTP. YTP was increased until a result was reached that was unsatisfactory. From the results in Table VIII, the maximum value of YTP was determined to be 1800 feet. This conclusion corresponds with the results in reference 13. Since the missile is symmetric, it was also concluded that moving YTP either right or left would give the same results.

The fifth run simulated a drop in the missile's altitude. ZTP was

RUN	XTP	YTP	ZTP
BASELINE	173552.5	0.0	0.0
1	173552.5	1000.0	0.0
2	173552.5	1500.0	0.0
3	173552.5	1800.0	0.0
4	173552.5	2000.0	0.0
5	173552.5	0.0	2000.0

INITIAL CONDITIONS

TABLE VII

RUN	XTP	YTP	ZTP	IMPACT TIME
BASLINE	234999.56	-.0506363	34999.34	28.825
1	234999.81	.1259258	34999.836	29.108
2	235000.19	.11479032	35000.32	29.124
3	235000.25	.15263242	35000.391	29.134
4	269802.0	2000.0	19705.00	35.0
5	234999.63	.45691	35000.426	30.365

IMPACT RESULTS

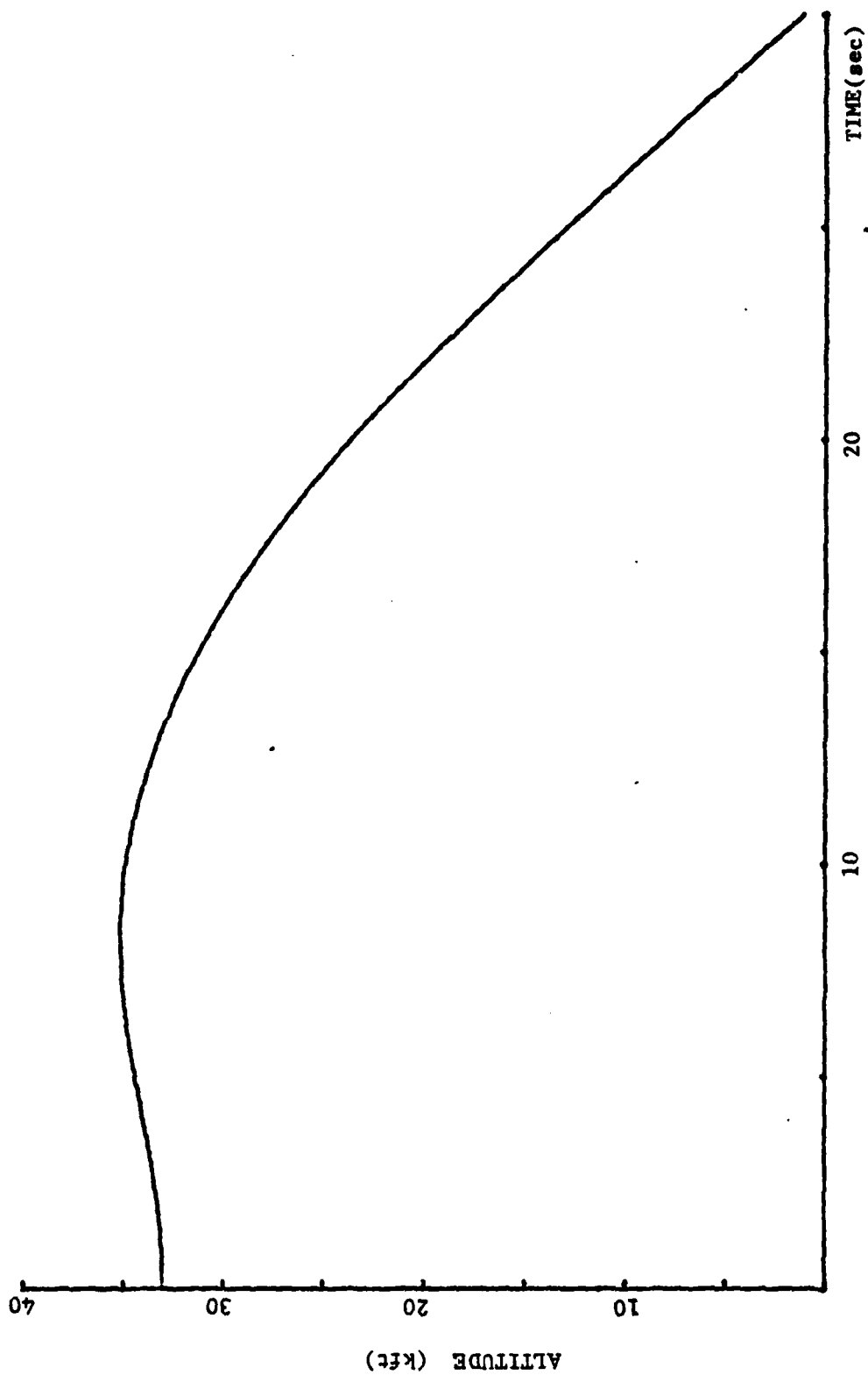
TABLE VIII

inputed as 2000.0 feet. As the simulation progressed, the missile developed the necessary commands to climb and regain the desired cruise altitude (Figure 15). It then commenced its terminal dive. The target was detected, acquired, and impact followed. This initial condition modification produced the largest miss distance (0.457 ft.).

Figure 16 was presented to show the relative locations of the miss distances for each change. Table VIII reveals that up until 1800 feet, changes to YTP created very little variation in the miss distance. It should be noted that the larger the displacement became, the greater the time until impact. The increase in time was necessary to allow the missile to acquire the target and then compute the required actuator commands to impact the target. This concluded the investigation of the effects of initial displacement error on target miss distance.

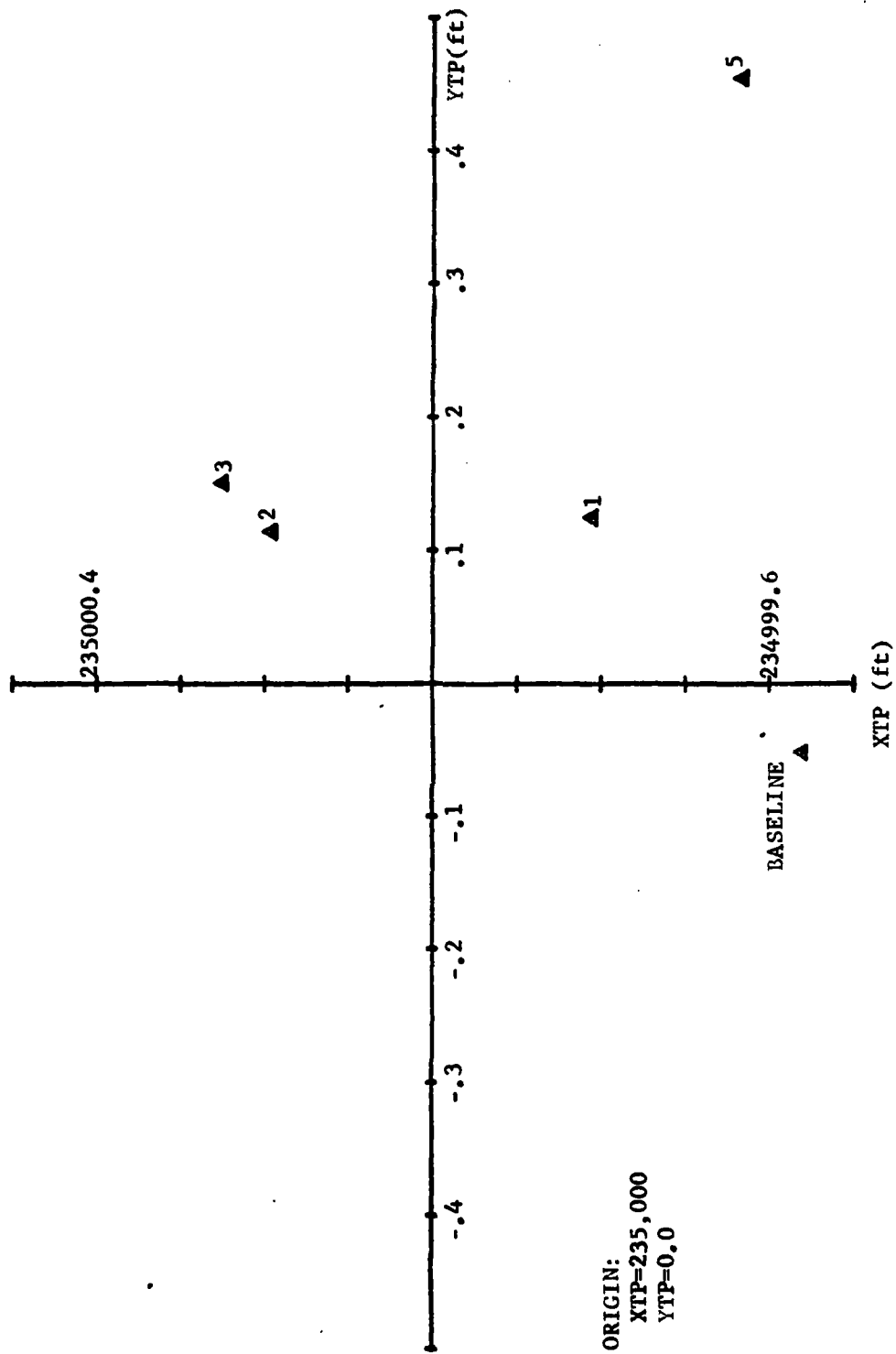
The idea behind changing the cruise altitude was to try and simulate a sea skimming profile. RAMJET contains tables that allow for four cruise altitudes. Of these four altitudes, the lowest (500 ft) was chosen even though it is high for a sea-skimmer. To run this simulation only two input data card changes were required. HO(414) and HREF(501) had to be set equal to the desired altitude. The resultant flight path is shown in Figure 17.

The simulation produced an error-free output, but at first glance the results appeared unacceptable. Still trying to compare miss distances, the downrange distance (XTP) was found to be 197916 feet. Comparing this to the terminal baseline (234999) resulted in an extreme error. It was then realized that the missile must expend more fuel at this altitude to attain the same speed. Therefore, the results could be correct. As further verification of the correctness of the run, it was assumed that the missile weight at impact should be fairly equal. The



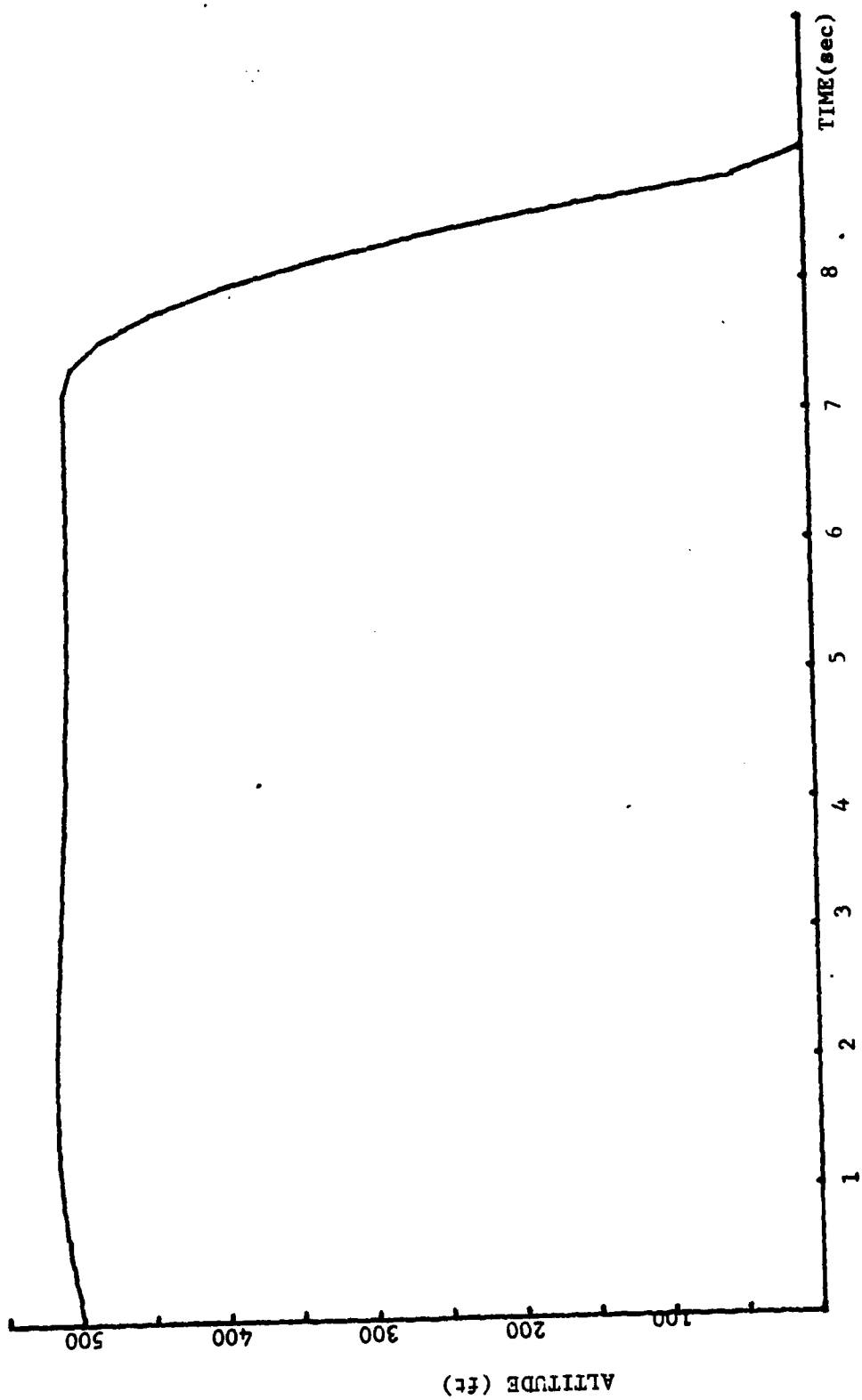
ALTITUDE VS. TIME (TERMINAL - ZTP)

FIGURE 15



IMPACT RESULTS

FIGURE 16



ALTITUDE VS. TIME (SEA-SKIMMER)

FIGURE 17

simulation impact weight was 1126.34 lbs while the terminal baseline weighed 1113.12 lbs. Since no conflicting information could be found in reference 12, it was concluded that this simulation was correct.

The final flight disturbance investigated was the addition of random noise to the missile homing seeker. This simulation proved to be unsuccessful due to invalid input format. The information describing the process is brief and difficult to understand. Further information from NWC China Lake is required to be able to successfully run simulations with random noise.

With the completion of these modifications, many unanswered problems and questions still exist. The two most critical problems concern the input of random noise generators and the missile exceeding the angle of attack limitation when using ENGINE for cruise propulsion. However, the simulations did show that the MOD6DF program runs correctly at alternate cruise altitudes and with initial displacement errors.

VI. CONCLUSION

The MOD6DF computer program from NWC China Lake was converted to operate on the IBM-360 computer at the Naval Postgraduate School. The program would only function properly when using the simplified ramjet model. When this model was not used, the missile angle of attack exceeded the maximum limit of ten degrees. This error caused the ramjet engine to flame out.

Target impact errors for the terminal guidance problem were investigated when the initial displacement was modified. These modifications demonstrate the missile's accuracy when removed from the ideal flight path. The results also point out that if the target falls within the seeker search pattern, target impact will inevitably happen.

Random noise generation is possible with the MOD6DF program. However, more information discussing the parameters required to develop the noise is necessary. Additionally, sample noise inputs should be obtained that reflect the alteration to the noise subroutines.

This research involved the preliminary investigation of the MOD6DF program. The program has many possible areas, concerning guidance and control of tactical missiles, which could be developed for future study. These areas not only include the unresolved problems encountered during this research. Additionally, reference 14 and 15 contain many examples of possible advanced guidance concepts.

COMPUTER OUTPUT

INFL1	011	G1
INFL2	021	G3
INFL3	031	G5
INFL4	041	G5
INFL5	051	G5
INFL6	061	G5
INFL7	071	G5
INFL8	081	G5
INFL9	091	G5
INFL10	101	G5
INFL11	111	G5
INFL12	121	G5
INFL13	131	G5
INFL14	141	G5
INFL15	151	G5
INFL16	161	G5
INFL17	171	G5
INFL18	181	G5
INFL19	191	G5
INFL20	201	G5
INFL21	211	G5
INFL22	221	G5
INFL23	231	G5
INFL24	241	G5
INFL25	251	G5
INFL26	261	G5
INFL27	271	G5
INFL28	281	G5
INFL29	291	G5
INFL30	301	G5
INFL31	311	G5
INFL32	321	G5
INFL33	331	G5
INFL34	341	G5
INFL35	351	G5
INFL36	361	G5
INFL37	371	G5
INFL38	381	G5
INFL39	391	G5
INFL40	401	G5
INFL41	411	G5
INFL42	421	G5
INFL43	431	G5
INFL44	441	G5
INFL45	451	G5
INFL46	461	G5
INFL47	471	G5
INFL48	481	G5
INFL49	491	G5
INFL50	501	G5
INFL51	511	G5
INFL52	521	G5
INFL53	531	G5
INFL54	541	G5
INFL55	551	G5
INFL56	561	G5
INFL57	571	G5
INFL58	581	G5
INFL59	591	G5
INFL60	601	G5
INFL61	611	G5
INFL62	621	G5
INFL63	631	G5
INFL64	641	G5
INFL65	651	G5
INFL66	661	G5
INFL67	671	G5
INFL68	681	G5
INFL69	691	G5
INFL70	701	G5
INFL71	711	G5
INFL72	721	G5
INFL73	731	G5
INFL74	741	G5
INFL75	751	G5
INFL76	761	G5
INFL77	771	G5
INFL78	781	G5
INFL79	791	G5
INFL80	801	G5
INFL81	811	G5
INFL82	821	G5
INFL83	831	G5
INFL84	841	G5
INFL85	851	G5
INFL86	861	G5
INFL87	871	G5
INFL88	881	G5
INFL89	891	G5
INFL90	901	G5
INFL91	911	G5
INFL92	921	G5
INFL93	931	G5
INFL94	941	G5
INFL95	951	G5
INFL96	961	G5
INFL97	971	G5
INFL98	981	G5
INFL99	991	G5
INFL100	1001	G5

W. F. L. S. T. I.
C. R. A. T.
C. G. I.
F. S. T. H.
N. L. T. H.

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LA 33
LA 34

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FMG
FMG
FMG

FM 6V
CMGZD
LCMGZ
LLMGZ

CMCZ
 YH TSD
 BITHYS
 BITHYS

25150

FLVX

:LVX
 VX
 FLX
 FLX

X
L V Y
L V Y
L V Y

THE UNIVERSITY OF CHICAGO

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TIME	TP-CST	WIGHT	X(TP)	W(TP)	Y(TP)	Y(TP)
0.40555950F-02	C.1141750F-04 C.2504340F-01 C.0 C.0 C.0	0.1152555F-14 0.1152555F-05 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-06 C.0 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02
0.40555952F-00	C.1152555F-04 C.1152555F-05 C.1152555F-04 C.1152555F-01 C.1152555F-02	0.1152555F-14 0.1152555F-05 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-06 C.0 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02
0.40555951F-00	C.1152555F-04 C.1152555F-05 C.1152555F-04 C.1152555F-01 C.1152555F-02	0.1152555F-14 0.1152555F-05 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-06 C.0 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02
0.40555954F-00	C.1152555F-04 C.1152555F-05 C.1152555F-04 C.1152555F-01 C.1152555F-02	0.1152555F-14 0.1152555F-05 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-06 C.0 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02
0.40555953F-00	C.1152555F-04 C.1152555F-05 C.1152555F-04 C.1152555F-01 C.1152555F-02	0.1152555F-14 0.1152555F-05 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-06 C.0 0.1152555F-04 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02	0.1152555F-04 0.1152555F-01 0.1152555F-02 0.1152555F-01 0.1152555F-02

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COMPUTER PROGRAM

CD60010
MCD60020
MCD60030
MCD60040
MCD60050
MCD60060
MCD60070
MCD60100
MCD60120
MCD60130
MCD60140
MCD60150
MCD60160
MCD60170
MCD60200
MCD60210

CD60220
MCD60230
MCD60240
MCD60250
MCD60260
MCD60270
MCD60300
MCD60320
MCD60330
MCD60340
MCD60350
MCD60360
MCD60370
MCD60400
MCD60410
MCD60420
MCD60430
MCD60440
MCD60450
MCD60460
MCD60470
MCD60500
MCD60510
MCD60520

THIS IS THE MAIN MCD6CF PROGRAM

CMPCN C(3415), TEMPS(1500)
CEQUIVALENCE C(315), N
CEQUIVALENCE C(2911), HMIN
CEQUIVALENCE C(2912), HMAX
CEQUIVALENCE C(2913), CER(1)
CEQUIVALENCE C(3014), VAR(1)
CEQUIVALENCE C(3115), EL(1)
CEQUIVALENCE C(3215), EL(1)
CEQUIVALENCE C(3316), TPL(1)
CEQUIVALENCE C(932), T
CEQUIVALENCE C(2904), KSTEP), (C(2905), STEP)
CEQUENSICN IPL(100)
CEQUENSICN DER(101)
CEQUENSICN VAR(101)
CEQUENSICN EL(100)
CEQUENSICN EU(100)
DIMENSION N=N
N=M

1001 CALL ZFC
1002 CALL CINPT1
1003 LSTEP = SUELI
1004 CALL AXI
1005 CALL SUBL2
DO 60 J = 1, N
EL(I-1) = C(J+1)
EU(I-1) = C(J+2)
VAR(I-1) = C(J+3)
CER(I) = C(J)
CALL VAR(1) AUXSUB
CALL AMK
DO 50 I = 2, N
J = IPL(I-1)
C(J+3) = VAR(I)
T = VAR(1)
CALL CLEL3
IF (KSTEP - EQ, 1) GC TC 1007
IF (KSTEP - 1) 70, 1007, 7C
CALL RESET
GO TC 1000, 1001, 1002, 1003, 1004, 1005, 1006, 1007, 1008, 1009, 1010),

MCD60530
 MCD60540
 MCD60545
 MCD60550

1 LSTEP
 1010 CALL EXIT
 STCP
 END

C C C C

SUBROUTINE ZERO

COMMON C(2415)
 DO 1 KLEAF = 1, 4915
 1 C(KLEAF) = 0.0
 RETURN
 END

C C C C C C C C

SUBROUTINE QINPT1

BASIC INFLT SUBROUTINE QINPT1
 SUBROUTINE QINPT1 IS THE BASIC INPUT SUBROUTINE

DIMENSION LISTNO(50), VALUE(50)
 DIMENSION SUBNO(99), IR(2), VR(2)
 DIMENSION RNMNO(50)
 DIMENSION ALPHA(4), CNAME1(50), CNAME2(50), CNAME3(50), OUTNC(50)
 DIMENSION MCCNO(99)
 DIMENSION STATNO(100)
 COMMON C(2415)

REAL MCDNC
 INTEGER CLTNC
 INTEGER RADMNO
 INTEGER STATNG
 EQUIVALENCE (C(2442), LOSTAT)
 EQUIVALENCE (C(2200), STATNO(1)), (C(2441), NOSTAT)
 EQUIVALENCE (C(2801), NOSUB), (C(2802), SUBNO(1)), (C(2663), IR(1)),
 1 (C(2661), VR(1))
 EQUIVALENCE (C(2701), NCMOD)
 EQUIVALENCE (C(2661), NCMOUT)
 EQUIVALENCE (C(2448), NORNDM)
 EQUIVALENCE (C(2300), NOLIST), (C(2301), LISTNO(1)), (C(2351),
 1 VALUE(1))
 EQUIVALENCE (C(2500), CUTNO(1))
 EQUIVALENCE (C(2550), CNAME1(1))
 EQUIVALENCE (C(2600), CNAME2(1))
 EQUIVALENCE (C(2150), CNAME3(1))
 EQUIVALENCE (C(2450), RADMNO(1))
 EQUIVALENCE (C(2702), MCDNC(1))
 JAR = C

C INP0030
 C INP001C
 C INP0020
 C INP0230
 C INP0240
 C INP0250
 C INP030C
 C INP0040
 C INP031C
 C INP032C
 C INP0330
 C INP034C
 C INP005C
 C INP011C
 C INP012C
 C INP0130

C INP0350


```

1 READ(5,2) IR(1),ALPHA(1),ALPHA(2),ALPHA(3),ALPHA(4),IR(2),VR(1),
1 VR(2)
1 WRITE(6,2) IR(1),ALPHA(1),ALPHA(2),ALPHA(3),ALPHA(4),IR(2),VR(1),
1 VR(2)
2 FORMAT(12,2X,4A4,15,5X,2E15.8)
3 IF (IR(1) .NE. 0) GC TO 7
4 IF (IR(1)) 7,18,7
18 REMAIN(1) - 1.
19 I3 = VR(2)
20 IF (I2) 11,15,14
21 DO 8 I = 1,12
22 READ (11,10) J,X
23 CO 9 I = 1,13
24 READ (11,2) J,X
25 C(J) = X
26 FCPRAT (15,E15.9)
27 GO TO 1
28 JAR = 1
29 GO TO 1
30 IF (IR(1) .NE. 1) GC TO 3
31 IF (IR(1) - 1) 3,19,3
32 NOSUB = NCSUB + 1
33 SUBNC(NCSUB) = IR(2)
34 GO TO 1
35 IF (IR(1) .NE. 2) GC TO 4
36 IF (IR(1) - 2) 4,20,4
37 NOMOD = NCMOD + 1
38 MODNC(NCMOD) = IR(2)
39 GO TO 1
40 IF (IR(1) .NE. 3) GC TO 5
41 IF (IR(1) - 3) 5,21,5
42 L = IR(2)
43 C(L) = VR(1)
44 IF (JAR .EQ. 1) WRITE (11,10)L,VR(1)
45 IF (JAR - 1) 23,22,23
46 WRITE (11,10)L,VR(1)
47 IF (VR(2) .EQ. 0) GC TO 1
48 IF (VR(2)) 24,1,24
49 NOLIST = NOLIST + 1
50 LISTNC(NCLIST) = L
51 VALUE(NCLIST) = VR(1)
52 GO TO 1
53 IF (IR(1) .NE. 4) GC TO 6
54 IF (IR(1) - 4) 6,25,6
55 ACCUT = ACCUT + 1
56 CNAME1(NCCLT) = ALPHA(2)

```

```

CINP0410
CINP042C
CINP043C
CINP0440
CINP045C
CINP0460
CINP0470
CINP050C
CINP0510
CINP052C
CINP053C
CINP0540
CINP055C
CINP056C
CINP0570
CINP060C
CINP0610
CINP062C
CINP063C
CINP064C
CINP065C
CINP0660
CINP0670
CINP070C
CINP071C
CINP072C
CINP073C
CINP0740
CINP075C
CINP076C
CINP0770
CINP100C
CINP1010
CINP102C
CINP103C
CINP1040
CINP105C
CINP1060
CINP1070
CINP110C
CINP111C
CINP112C

```



```

GO TC 1
6 CALL RNCM1
GO TC 1
7 CALL ALXA1
GO TC 1
8 CALL ALXB1
GO TC 1
9 CALL ALXC1
10 CONTINUE
11 RETURN
END

```

CC C

SUBROUTINE SUBL2

```

DIMENSION SUBNO(99)
COMMON C(3415)
EQUIVALENCE (C(2801),NCSLB)
DO 1 I = 1, NCSUB
J = SUBNO(I)
GO TO (1, 2, 3, 4, 5, 6, 7, 8, 9), J
2 CALL INFT2
GO TC 1
3 CALL CLFT2
GO TC 1
4 CALL STGE2
GO TC 1
5 CALL CNTR2
GO TC 1
6 CALL RNCM2
GO TO 1
7 CALL ALXA2
GO TC 1
8 CALL ALXB2
GO TC 1
9 CALL ALXC2
10 CONTINUE
11 RETURN
END

```

CC C

SUBROUTINE SUBL3

```

DIMENSION SUBNO(99)
COMMON C(3415)

```

SUBL0200
SUBL0210
SUBL0220
SUBL0230
SUBL0240
SUBL0250
SUBL0260
SUBL0270
SUBL0280
SUBL0290
SUBL0300
SUBL0310
SUBL0320

SUBL0010
SUBL0050
SUBL0020
SUBL0030
SUBL0060
SUBL0070
SUBL0100
SUBL0110
SUBL0120
SUBL0130
SUBL0140
SUBL0150
SUBL0160
SUBL0170
SUBL0200
SUBL0210
SUBL0220
SUBL0230
SUBL0240
SUBL0250
SUBL0260
SUBL0270
SUBL0300
SUBL0310
SUBL0320

SUBL0010
SUBL0050
SUBL0020

SURL0030
SURL006C
SURL0070
SURL0100
SURL0110
SURL0120
SURL0130
SURL0140
SURL0150
SURL0160
SURL0170
SURL0200
SURL0210
SURL0220
SURL0230
SURL0240

SURL0250
SURL0260
SURL0270
SURL0300
SURL0310
SURL0320

ALXI0010
ALXI0060
ALXI0020
ALXI0070
ALXI0030

ALXI0050
ALXI0100
ALXI0110
ALXI0120
ALXI0130
ALXI0140
ALXI0150
ALXI0160
ALXI0170
ALXI0200
ALXI0210
ALXI0220

```

EQUIVALENCE (C(2801),NOSUB)
EQUIVALENCE (C(2802),SUENO(1))
DO I=1,NOSUB
  J=SUENO(I)
  GO TC (1,2,3,4,5,6,7,8,9),J
2 CALL INPT3
3 CALL CLFT3
4 CALL STGE3
5 CALL CNTR3
6 CALL RNCM3
7 CALL ALX3
8 CALL ALXB3
9 CALL ALXC3
1 CONTINUE
1 RETURN
1 END

```

```

SUBROUTINE ALXI
DIMENSION MCDNO(99)
COMMON C(3415)
REAL MCDNO
EQUIVALENCE (C(2701),ACMOD)
EQUIVALENCE (C(2702),MCDNO(1))
EQUIVALENCE (C(2659),CNCE)
EQUIVALENCE (C(3315),N)
N=1
CNCE=0
DO I=1,N
  L=MCDNO(I)
  GO TC (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24,25,26,27,28,29,30,31,32,33,34,35,36,37),L
1 CALL AI
2 GO TC AI
3 CALL A2I
4 GO TC A2I
5 GO TC A2I
6 GO TC A2I

```

CC C

XI023C
 AXI024C
 AXI025C
 AXI026C
 AXI027C
 AXI028C
 AXI029C
 AXI030C
 AXI031C
 AXI032C
 AXI033C
 AXI034C
 AXI035C
 AXI036C
 AXI037C
 AXI038C
 AXI039C
 AXI040C
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 AXI074C
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 AXI076C
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 AXI078C
 AXI079C
 AXI080C
 AXI081C
 AXI082C

5 CALL A4I
 6 GO TC I
 7 CALL A5I
 8 GO TC I
 9 CALL C1I
 10 GO TC I
 11 CALL C2I
 12 GO TC I
 13 CALL C3I
 14 GO TC I
 15 CALL C4I
 16 GO TC I
 17 CALL C5I
 18 GO TC I
 19 CALL C6I
 20 GO TC I
 21 CALL C7I
 22 GO TC I
 23 CALL C8I
 24 GO TC I
 25 CALL C9I
 26 GO TC I
 27 CALL D1I
 28 GO TC I
 29 CALL D2I
 30 GO TC I
 31 CALL D3I
 32 GO TC I
 33 CALL D4I
 34 GO TC I
 35 CALL D5I
 36 GO TC I
 37 CALL D6I
 38 GO TC I
 39 CALL D7I
 40 GO TC I
 41 CALL D8I
 42 GO TC I
 43 CALL D9I
 44 GO TC I
 45 CALL E1I
 46 GO TC I
 47 CALL E2I
 48 GO TC I
 49 CALL E3I
 50 GO TC I
 51 CALL E4I
 52 GO TC I
 53 CALL E5I
 54 GO TC I
 55 CALL E6I
 56 GO TC I
 57 CALL E7I
 58 GO TC I
 59 CALL E8I
 60 GO TC I
 61 CALL E9I
 62 GO TC I
 63 CALL F1I
 64 GO TC I
 65 CALL F2I
 66 GO TC I
 67 CALL F3I
 68 GO TC I
 69 CALL F4I
 70 GO TC I
 71 CALL F5I
 72 GO TC I
 73 CALL F6I
 74 GO TC I
 75 CALL F7I
 76 GO TC I
 77 CALL F8I
 78 GO TC I
 79 CALL F9I
 80 GO TC I
 81 CALL G1I
 82 GO TC I
 83 CALL G2I
 84 GO TC I
 85 CALL G3I
 86 GO TC I
 87 CALL G4I
 88 GO TC I
 89 CALL G5I
 90 GO TC I
 91 CALL G6I
 92 GO TC I
 93 CALL G7I
 94 GO TC I
 95 CALL G8I
 96 GO TC I
 97 CALL G9I
 98 GO TC I
 99 CALL H1I
 100 GO TC I

[illegible]

```

      C(J+1) = VAR(I)
      C(J+2) = VAR(I)
      DO 1 I=1,NCMCC
      L = MCONC(I)
      GO TO (1,2,3,4,
      123,24,45,26,27,
      2,CALL A)
      GO TO 1

```

```

L = MGENC(I)
GO TO (I, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22,
23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37), L

```

0310
 0320
 0330
 0340
 0350
 0360
 0370
 0410
 0420
 0430
 0440
 0450
 0460
 0470
 0500
 0510
 0520
 0530
 0540
 0550
 0560
 0570
 0600
 0610
 0620
 0630
 0640
 0650
 0660
 0670
 0700
 0710
 0720
 0730
 0740
 0750
 0760
 0770
 1000
 1010
 1020
 1030
 1040
 1050
 1060
 1070
 1100

3 CALL A1
 4 GO CALL A1
 5 GO CALL A1
 6 GO CALL A1
 7 GO CALL C1
 8 GO CALL C1
 9 GO CALL C1
 10 GO CALL C1
 11 GO CALL C1
 12 GO CALL C1
 13 GO CALL C1
 14 GO CALL C1
 15 GO CALL C1
 16 GO CALL C1
 17 GO CALL C1
 18 GO CALL C1
 19 GO CALL C1
 20 GO CALL C1
 21 GO CALL C1
 22 GO CALL C1
 23 GO CALL C1
 24 GO CALL C1
 25 GO CALL C1
 26 GO CALL C1


```

APRK0223C
APRK0224C
APRK0225C
APRK0226C
APRK0227C
APRK0228C
APRK0229C
APRK0230C
APRK0231C
APRK0232C
APRK0233C
APRK0234C
APRK0235C
APRK0236C
APRK0237C
APRK0238C
APRK0239C
APRK0240C
APRK0241C
APRK0242C
APRK0243C
APRK0244C
APRK0245C
APRK0246C
APRK0247C
APRK0248C
APRK0249C
APRK0250C
APRK0251C
APRK0252C
APRK0253C
APRK0254C
APRK0255C
APRK0256C
APRK0257C
APRK0258C
APRK0259C
APRK0260C
APRK0261C
APRK0262C
APRK0263C
APRK0264C
APRK0265C
APRK0266C
APRK0267C
APRK0268C
APRK0269C
APRK0270C
APRK0271C
APRK0272C
APRK0273C
APRK0274C
APRK0275C
APRK100C
APRK101C
APRK102C

```

```

1 IF (CNCE) 2,1,2
  CNCE = 1
  N = NI - 1
  CPT = 0
  P1 = 0.2516666666666667
  P2 = 0.4583333333333333
  P3 = 0.5416666666666667
  P4 = 0.375
  C2 = 0.7516666666666667
  C3 = 0.2083333333333333
  C4 = 0.0416666666666667
  KCUNT = 0
  N1 = N
  J2 = J1 + N1
  J3 = J2 + N1
  J4 = J3 + N1
  J5 = J4 + N1
  J6 = J5 + N1
  J7 = J6 + N1
  J8 = J7 + N1
  J9 = J8 + N1
  J10 = J9 + N1
  J11 = J10 + N1
  J12 = J11 + N1
  J13 = J12 + N1
  J14 = J13 + N1
  J15 = J14 + N1
  IF (CPT) 60,49,60
  IF (OPT) 60,49,60
  IF (DELT) 50,200,50
  IF (DELT) 50,200,50
  KOUNT = C
  STAFF FLNGE-KUTTA INTEGRATION.
  COMPUTE KC
  CONTINUE
  CO 25 I=1,N1
  K5 = J15 + 1
  IF (SAGL(T(K5)) - NE, V(I+1)) T(K5) = V(I+1)
  IF (SAGL(T(K5)) - V(I+1)) T(K5) = V(I+1)
  24 T(K5) = V(I+1)
  25 CONTINUE
  IF (SAGL(TME) - NE, V(I)) TME = V(I)
  TME = V(I)
  26 KOUNT = KCUNT + 1
  27 CC 80 I=1,N1
  70 KO = J7 + 1

```

ARK1030
 ARK1040
 ARK1050
 ARK1060
 ARK1070
 ARK1100
 ARK1110
 ARK1120
 ARK1130
 ARK1140
 ARK1150
 ARK1160
 ARK1170
 ARK1200
 ARK1210
 ARK1220
 ARK1230
 ARK1240
 ARK1250
 ARK1260
 ARK1270
 ARK1300
 ARK1310
 ARK1320
 ARK1330
 ARK1340
 ARK1350
 ARK1360
 ARK1370
 ARK1400
 ARK1410
 ARK1420
 ARK1430
 ARK1440
 ARK1450
 ARK1460
 ARK1470
 ARK1500
 ARK1510
 ARK1520
 ARK1530
 ARK1540
 ARK1550
 ARK1560
 ARK1570
 ARK1600
 ARK1610
 ARK1620

```

      80 T(K0)=C(1)*D(I+1)
      C
      C
      C      COMPUTE K1
      C      CELT=C(.5*C(1)
      C      TME=CELT+TME
      C      V(1)=TME
      C      DO 90 I=1,N1
      C      K0=J7+I
      C      K1=J11+I
      C      K2=J12+I
      C      K3=J13+I
      C      K5=J15+I
      C      T(I)=C(I+1)
      C      T(K1)=T(K2)
      C      T(K2)=T(K3)
      C      T(K3)=T(K5)
      C      T(K5)=T(K5) +0.5*T(K0)
      C      V(I+1)=T(K5)
      C      CALL AUXSLE
      C      DO 100 I=1,N1
      C      K1=J8+I
      C      T(K1)=C(1)*D(I+1)
      C      100 T(K1)=C(1)*D(I+1)
      C
      C      CCMPLTE K2
      C      DO 110 I=1,N1
      C      K5=J15+I
      C      K1=J8+I
      C      K0=J7+I
      C      T(K5)=T(K5) +0.5*(T(K1)-T(K0))
      C      V(I+1)=T(K5)
      C      CALL AUXSLE
      C      DO 120 I=1,N1
      C      K2=J6+I
      C      T(K2)=C(1)*C(I+1)
      C      120 T(K2)=C(1)*C(I+1)
      C
      C      CCMPLTE K3
      C      TME=CELT+TME
      C      V(1)=TME
      C      DO 130 I=1,N1
      C      K5=J15+I
      C      K2=J6+I
      C      K1=J8+I
      C      T(K5)=T(K5) +T(K2)-0.5*T(K1)
      C      V(I+1)=T(K5)
      C      CALL AUXSLE
      C      130
  
```

```

DO 140 I=1,N1
K3=J10+I
T(K3)=C(I)*D(I+1)
CC
C
COMPLETE VALUE OF FUNCTION.
CC
DO 150 I=1,N1
K0=J7+I
K1=J8+I
K2=J9+I
K3=J10+I
K5=J15+I
T(K5)=T(K5)+O.16666666666666667*
1(T(KC))+T(K1)+T(K2)+T(K3)+T(K5)
V(I+1)=T(K5)
CC
CONTINUE
170
CALL ALCXSUB
CO J180 I=1,N1
K5=J1+I
K0=J2+I
K1=J3+I
K2=J4+I
K3=J5+I
K4=J6+I
T(K4)=T(K4)+(K3)
T(K3)=T(K3)+(K2)
T(K2)=T(K2)+(K1)
T(K1)=T(K1)+(K0)
T(KC)=T(KC)+(K5)
T(I)=T(I)+(I+1)
CONTINUE
180
CONTINUE
190
RETURN
CC
CC
DO ACAMS-MCULTON INTEGRATION
CC
CONTINUE .LT. 3) GO TO 60
IF (KCLNT - 3) 60,201,201
IF (KCLNT = KCLNT + 1
201
COUNT = C(1)*.5
DO 210 I=1,N1
K0=J7+I
K1=J8+I
K2=J9+I
K3=J10+I

```


APRK317C
APRK320C
APRK321C
APRK322C
APRK323C
APRK324C
APRK325C
APRK326C
APRK327C
APRK330C
APRK331C
APRK332C
APRK333C
APRK334C
APRK335C
APRK336C
APRK337C
APRK340C
APRK341C
APRK342C
APRK343C
APRK344C
APRK345C
APRK346C
APRK347C
APRK350C
APRK351C
APRK352C
APRK353C
APRK354C
APRK355C
APRK356C
APRK357C
APRK360C
APRK361C
APRK362C
APRK363C
APRK364C
APRK365C
APRK366C
APRK367C
APRK370C
APRK371C
APRK372C
APRK373C
APRK374C
APRK375C
APRK376C

```

240      K5=J5+I
        T(K1)=T(K1)
        T(K2)=T(K2)
        C(1)=C(1)+C(1)
        KOUNT=4
        DELT=.5*C(1)
        GO TC 200

C      SET-UP FOR HALVING STEP SIZE.
C
C      CONTINUE
        IF(KCOUNT .LE. 4) GO TO 250
        IF(KCOUNT .GT. 4) 350,350,261
        TIME=TIME-C(1)
        V(1)=TAE
        D(1)=DELT
        GO 265 I=1,N1
        K0=J7+I
        K1=J1+I
        K2=J2+I
        K3=J3+I
        K5=J15+I
        T(K5)=T(KC)
        V(I+1)=T(KC)
        T(K3)=T(K2)+0.5*(T(K1)-T(K2))
        T(K2)=T(K1)
        T(K1)=T(K1)+0.5*(T(I)-T(K1))
        KOUNT=4
        GO TC 200

C      INTEGRATION IS FINISHED. SET UP DERIVATIVES AND EXIT.
C
C      300      CO 310 I=1,N1
        K5=J15+I
        K0=J8+I
        T(K5)=T(K0)
        V(I+1)=T(KC)
        GO TC 170
        CCATINLE
C
C      310      RETURN TO 3RD RK INTEGRATION AND RESTART
C
C      350      CO 360 I=1,N1
        K5=J15+I
        K1=J1+I
        T(K5)=T(K1)

```

APRK377C
APRK4000
APRK401C
APRK402C
APRK403C
APRK404C
APRK4050

36C V(I+1)=T(K1)
TME=TME-C(1)*4.
V(1)=TME
V(1)=CELT
CALL AUXSUE
GO TC 5C
END

CC

SUBROUTINE PROCES
RETURN
END

CC

SUBROUTINE RESFT

COMMON C(3415)
EQUIVALENCE (C(2300),NOLIST),(C(2301),LISTNC(1)),(C(2351),
1 VALUE(1))
EQUIVALENCE (C(2675),KRUN)
DIMENSION LISTN(50),VALUE(50)
IF(NOLIST.EQ.0) RETURN
DO 1 I=1,NCLIST
J=LISTN(I)
C(I)=VALUE(I)
1 KRUN=KRUN+1
RETURN
END

CC

SUBROUTINE INPT1

INPT001C

COMMON C(3415)
COMMON /CFLS/ ENG(30),IENG(15)
NAMELIST /MCNT/ ENG,IENG
EQUIVALENCE (C(2675),KRUN)
FLG1=0.
IF (KRUN.GT.0) GO TC 100
READ (5,MCNT)
WRITE (6,MCNT)
RETURN
10C END

F 96

F 106
F 108

CC

SUBROUTINE INPT2

INPT001C


```

C
C
SUBROUTINE CLPT3
CUTPLT SUBROUTINE CUT3
DIMENSION B(50),OUTNO(50),ONAME1(50),ONAME2(50)
COMMON C(215)
INTEGER CUTCNT,PGCNT,CUTNO(11)
EQUIVALENCE (C(2500),CUTNO(11))
EQUIVALENCE (C(2550),ONAME1(11))
EQUIVALENCE (C(2600),ONAME2(11))
EQUIVALENCE (C(2150),ONAME3(11))
EQUIVALENCE (C(2660),DTCNT)
EQUIVALENCE (C(2661),PGCNT)
EQUIVALENCE (C(2662),PCNT)
EQUIVALENCE (C(2667),ITCNT), (C(2668),PCNT), (C(2669),CPP)
EQUIVALENCE (C(2932),T)
EQUIVALENCE (C(2913),DER)
EQUIVALENCE (C(2670),TAP)
EQUIVALENCE (C(10290),XTP), (C(10298),YTP), (C(10306),ZTP)
EQUIVALENCE (C(3400),PUNCH)
EQUIVALENCE (C(0521),TFT)
EQUIVALENCE (C(0522),PST)
EQUIVALENCE (C(0523),PHI)
EQUIVALENCE (C(0554),AXECI)
EQUIVALENCE (C(0555),AYECI)
EQUIVALENCE (C(0556),AZECI)
EQUIVALENCE (C(0577),VXECI)
EQUIVALENCE (C(0552),VZECI)
EQUIVALENCE (C(0547),XECI)
EQUIVALENCE (C(0548),YECI)
EQUIVALENCE (C(0549),ZECI)
IF (ITCNT - GT. 6) GC TC 7
IF (ITCNT - 6) 10,10,7
1C ITCNT = ITCNT + 1
WRITE (6,6) (1,C(1),C(1+1),C(1+2),C(1+3),C(1+4),C(1+5),C(1+6),
1 C(1+7),I=1,2415,8)
6 FORMAT (1F11/15,2X,RE14.7)
PGCNT = 1
7 CCNT INCL
8 IF (IT - LT. PCNT) RETURN
8 IF (IT - PCNT) 12,9,9
12 REILRN
9 PCNT=PGCNT+CPP
10 IF (PGCNT - 1) 3,1,3
10 IF (PGCNT - 1) 3,1,3
1 WRITE(6,2) (ONAME1(I),ONAME2(I),ONAME3(I), I = 1, NOOUT)

```

```

CLPT002C
CLPT001C
CLPT017C
CLPT003C
CLPT020C

CLPT0070
CLPT010C
CLPT011C
CLPT0120
CLPT013C
CLPT014C
CLPT0150
CLPT016C

CLPT0210
CLPT0220
CLPT023C
CLPT024C
CLPT025C
CLPT026C
CLPT027C

CLPT0340
CLPT0350
CLPT036C
CLPT040C
CLPT041C

```


STGE0640
STGE0650
STGE0660
STGE0670
STGE0700
STGE0710
STGE0720
STGE0730
STGE0740
STGE0750
STGE0760
STGE0770
STGE1000
STGE1010

CNTR0010
CNTR0020
CNTR0030

CNTR0010
CNTR0020
CNTR0030

CNTR0010
CNTR0020
CNTR0030

RNDM0010
RNDM0020
RNDM0030

C IF (K .NE. 0) END FILE K
C IF (K .NE. 0) REWIND K
C IF (K) 16,17,18
C 16 REWIND K
C 17 KSTEP = 2
C IF (LCSTAT .EQ. NCSTAT) GO TO 4
C IF (LCSTAT - NCSTAT) 18,4,18
C 18 DO 3 I = 1, NCSTAT
C L = LCSTAT + 1
C = STATNC(I)
C RMS(I) = C(N)
C RETURN
C 4 END

SUBROUTINE CNTR1
RETURN
END

SUBROUTINE CNTR2
RETURN
END

SUBROUTINE CNTR3
RETURN
END

SUBROUTINE RADM1
RETURN
END

SUBROUTINE RADM2
COMMON C(3415)
EQUIVALENCE (C(2443), RNFLG)
EQUIVALENCE (C(2446), ZN)
EQUIVALENCE (C(2448), NOFNDM)
EQUIVALENCE (C(2449), DELT)
EQUIVALENCE (C(2450), RNCMNO)
EQUIVALENCE (C(2913), DEF)
DIMENSION RNDMND(50)
INTEGER RNDMND

```

3 IF (ACENDM) 2,2,3
  RNFLG=CE
  CELT=CE
  DO 1 I=1,ACRNDM
    J=RNPMAC(I)
    C(J+5)=2.718281828**(-DER*C(J+4))
    C(J+6)=C(J+5)*SQRT(1.0-C(J+5)*C(J+5))
    ZN=C(J+1)
    Y=C(J)
    N=INT(Y)
    CALL RFG(N,X)
    C(J+7)=C(J+3)*X
    C(J+1)=ZN
  2 RETURN
  3 END

```

CC C

SUBROUTINE RNDM3

```

COMMON C(3415)
EQUIVALENCE (C(2443), RNFLG)
EQUIVALENCE (C(2444), RN)
EQUIVALENCE (C(2446), ZN)
EQUIVALENCE (C(2448), NCRNDM)
EQUIVALENCE (C(2449), DELT)
EQUIVALENCE (C(2450), RNDMAC)
EQUIVALENCE (C(2913), DER)
DIMENSION RNDMND(50)
INTEGER RNDMND
IF (ACENDM) 20,20,10 GC TC 8
IF (RNFLG=CE.1.0) GO TC 6
IF (RNFLG=CE.0.0) GO TC 6
J=RNPMAC(I)
X=(C(J+7)-C(J+5)*C(J+8))/C(J+6)
IF (RNFLG=CE.1.0) GC TC 5
RNFLG=-1-ER
GO TC 7
DELT=DELT+DER
C(J+5)=2.718281828**(-DELT*C(J+4))
C(J+6)=C(J+5)*SQRT(1.0-C(J+5)*C(J+5))
C(J+7)=C(J+6)*X+C(J+8)
RETURN
IF (CELT=EC.DER) GC TC 4
DO 3 I=1,ACRNDM
  J=RNPMAC(I)

```

10 8

7 5 4 2

```

3 C(J+5)=2.718281828*(-DER*C(J+4))
C(J+6)=C(J+3)*SQRT(1.0-C(J+5)*C(J+5))
DEL=DER
4 DO 1 I=1,NCRNDM
J=RNCRND(I)
Y=C(J)
ZN=C(J+1)
N=INT(V)
CALL RFG(N,X)
C(J+8)=C(J+7)
C(J+7)=C(J+6)*X+C(J+5)*C(J+7)
1 C(J+1)=ZN
20 RETURN
END

```

CC

```

SUBROUTINE AUXA1
RETURN
END

```

ALXA0010
ALXA0020
ALXA0030

CC

```

SUBROUTINE AUXA2
RETURN
END

```

CC

```

SUBROUTINE AUXA3
RETURN
END

```

CC

```

SUBROUTINE AUXB1
RETURN
END

```

ALXB0010
ALXB0020
ALXB0030

CC

```

SUBROUTINE AUXB2
RETURN
END

```

ALXB0010
ALXB0020
ALXB0030

CC

```

SUBROUTINE AUXB3
RETURN
END

```

ALXB0010
ALXB0020
ALXB0030

CC

```

SUBROUTINE AUXC1
RETURN

```

ALXC0010
ALXC0020

ALXC003C
ALXC001C
ALXC002C
ALXC003C
ALXC001C
ALXC002C
ALXC003C

```

END
SUBROUTINE ALXC2
RETURN
END
SUBROUTINE AUXC3
RETURN
END
SUBROUTINE RFG(N,X)
COMMON C(2415)
EQUIVALENCE (C(2446), ZN)
Y=FLCAT(N)
X=0.0
GENERATE UNIFORM RANCOV NO.(0 TO 1)
SUM FCR RAND NG(SIGMA=1,MEAN=0)
LN:FCR+ DIST FOR N=1
NORMAL DIST FOR LARGE N (12 OR GREATER)
DO 1 I=1,N
X=X+ZN-0.5
RNC=557.*ZN
ZN=RND-AINT(RNC)
1 X=SGRT(12./Y)*X
RETURN
END

```

```

SUBROUTINE AII
AERODYNAMIC FORCES AND MOMENTS INITIALIZATION MODULE AII
PGCY AXES
COMMON C(2415)
EQUIVALENCE (C(02CE), TSA )
EQUIVALENCE (C(0257), CTS )
EQUIVALENCE (C(025E), STS )
CTS = (CTS(TSA)
STS = SIN(TSA)
RETURN
END

```

```

C
C
C
SUBROUTINE A1
AERODYNAMIC FORCES AND MOMENTS MODULE A1 - BODY AXES

COMMON C(2415)
EQUIVALENCE
EQUIVALENCE(C(01101), S)
EQUIVALENCE(C(01111), CA)
EQUIVALENCE(C(01113), CY)
EQUIVALENCE(C(01115), CZ)
EQUIVALENCE(C(01116), CBRAR)
EQUIVALENCE(C(01118), CMCF)
EQUIVALENCE(C(01119), CNCF)
EQUIVALENCE(C(01120), CLPI)
EQUIVALENCE(C(01121), CM)
EQUIVALENCE(C(01122), CN)
EQUIVALENCE(C(01123), CLI)
EQUIVALENCE(C(01128), FXBA)
EQUIVALENCE(C(01129), FYBA)
EQUIVALENCE(C(01130), FZBA)
EQUIVALENCE(C(01131), CLBA)
EQUIVALENCE(C(01132), CNBA)
EQUIVALENCE(C(01133), CNBA)
EQUIVALENCE(C(02121), FBA)
EQUIVALENCE(C(02116), QBA)
EQUIVALENCE(C(02220), PBA)
EQUIVALENCE(C(02257), CTS)
EQUIVALENCE(C(02558), CCI)
EQUIVALENCE(C(05529), VAT)
CDS=CC*%CBAR
DIM=CBAR/(2*CMENTS*(PCDY AXES)
CLBA=QDS*CC*(CL+CLP*DIM*FBA)
CMEA=CC*CC*(CM+CMQ*DIM*QBA)
CNEA=CC*CC*(CN+CMR*DIM*PBA)
AERODYNAMIC FORCES (PCDY AXES)
FXBA=CCS*CA
FYBA=CCS*CY
FZBA=CCS*CZ
RETURN
END
C
C
SUBROUTINE A21
RETURN
C

```

END

SUBROUTINE A2

CAB - ZERC-LIFT BODY DRAG
CAC - DRAG DUE TO DEFLECTED CONTROL SURFACES
CAE+CAC
CZB - NORMAL FORCE DUE TO ANGLE OF ATTACK
CZC - NORMAL FORCE DUE TO FIN DEFLECTION
CYB - SIDE FORCE DUE TO SIDESLIP
CYC - SIDE FORCE DUE TO FIN DEFLECTION
CY - SIDE FORCE
CNG - PITCH DAMPING MOMENT
CAR - YAW DAMPING MOMENT
CLP - ROLL DAMPING MOMENT
CMB - PITCH MOMENT DUE TO ANGLE OF ATTACK
CNC - CONTROL SURFACE PITCH MOMENT
CMA+CNC
CAB - YAW MOMENT DUE TO SIDESLIP
CAC - CONTROL SURFACE YAW MOMENT
CNA+CNC
CLB - INDUCED ROLL MOMENT
CNC - CONTROL SURFACE ROLL MOMENT
CLB+CLC
CCL

COMMCN/APPLE/TM1(7), TM2(15), TM3(14), TM4(5), TETA1(7), TETA2(7),
1TETA3(6), TX11(2), TX12(10), TX13(5), TDELTA(4), TH1(3), TH2(2),
2TCZBC(1,2), TDCZP(14,7), TCYBC(7,10,6), TCMBC(7,5,7), TDCMF(14,7),
3TCZBC(15,2), TDC(15,2), TAD2(15), TCN8C(7,10,6), TCM01(15,4),
4TCMG2(15,4), TDCM0(15), TDCMCA(15), TPCMD(14,3), TCMQ(15), TPQ(14,3),
5TCLBC(7,10,6), TOLD(15), TPLD(14,3), TCLP(15), TPP(14,3), TDCYSP(3),
LTCCZSF(3), TDCMSP(3), TCCNSP(3), TH3(3), TFEJ(13), TFEJ(13)
COMMCN C(1,2415)
EQUIVALENCE (C(0016), DP)
EQUIVALENCE (C(0020), CC)
EQUIVALENCE (C(0024), CR)
EQUIVALENCE (C(0111), CA)
EQUIVALENCE (C(0113), CY)
EQUIVALENCE (C(0114), XI)
EQUIVALENCE (C(0115), CZ)
EQUIVALENCE (C(0116), CBAF)
EQUIVALENCE (C(0117), ETA)
EQUIVALENCE (C(0118), CMG)
EQUIVALENCE (C(0119), CNR)
EQUIVALENCE (C(0120), CLP)

[illegible]

```

VN=SQRT(VEA**2+WBA**2)
IF (VA-LT.C.03001) GT TC 10
XIR=ATAN2(VEA,WBA)
GO TC 20
1C XIR=C.C
20 XI=XIR/RAD
1C XI=XI
IF (XI.LT.C.C) XI1=-XI
XI2=XI1
IF (XI1.GE.90.) XI2=180.-XI1
C TABLE LOCK-UP,ALL PHASES
CCZP=0.0
CCMP=C.C
FMC=1.0
FNC=1.0
PLC=1.0
PR=1.0
PP=1.0
CCASEF=C.
CCASEF=C.
CCYSEF=C.
CCYSEF=C.
CCLSP=C.
CCLSP=C.
CCASP=C.
CCASP=C.
CCMENT CFFICIENTS
FITCHING MENT
CMRCC=TFREDL(AM,XI2,ETA,TM1,TX13,TETAL,TCMBC,7,5,7)
CCMUL=CCLLI(AM,TM2,TCMD,15)
CCMUL=CCMUL
CCMLL=CCMUL
CCMLR=CCMUL
CCMLA=CCLI(AM,TM2,TCMDA,15)
CCMURA=CCMULA
CCMLLA=CCMULA
CCMLRA=CCMULA
CCMC=CCLI(AM,TM2,TCMC,15)
YARING MENT
CNBC=TFREDL(AM,XI2,ETA,TM1,TX12,TETA3,TCNBC,7,10,6)
IF (XI1.GT.90.) CNBC=-CNBC
IF (XI1.LT.0.0) CNBC=-CNBC
CCNUL=CCMUL
CCNUL=CCMUL
CCNUL=CCMUL
CCNULB=CCMLA

```

AD-A085 147

NAVAL POSTGRADUATE SCHOOL MONTEREY CA
GUIDANCE AND CONTROL OF TACTICAL MISSILES.(U)
DEC 79 T A GROTE

F/G 16/2

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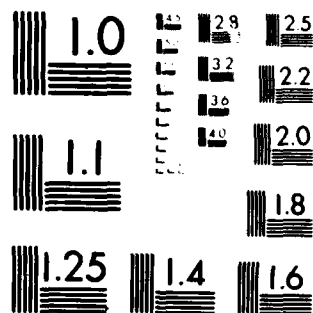
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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

```

CCNUFB=-CCMULA
CCNLFB=-CCMULA
CCNLRB=CCMULA
C
RCLLINC MCMENT
CLBC=TFRECL(AM,XI2,ETA,TM1,TXI2,TETA3,TCLBC,7,10,6)
IF (XI1.GT.90.) CLBC=-CLBC
IF (XI1.LT.0.) CLBC=-CLBC
CLC=COLI(AM,TM2,TCLD,15)
CLF=CLLI(AM,TM2,TCLF,15)
FCRCF CCEFFICIENTS
CZBCC=TFRECL(AM,XI2,ETA,TM1,TXI2,TETA3,TCYBC,7,2,7)
CYBC=TFRECL(AM,XI2,ETA,TM1,TXI2,TETA3,TCYBC,7,10,6)
IF (XI1.GT.50.) CYBC=-CYBC
IF (XI1.LT.0.) CYBC=-CYBC
CAC2=CLLI(AM,TM2,TCLD,15)
IF (T.GE.T3) GO TO 100
TAELE LICK-LF SEP AND BOOST PHASE
C
ZERC=LIFT CRAG
CDO=STLLIA(TM2,TH2,TCDB,AM,H,15,2)
IF (T.LT.T1) CDO=CCC+.08
C
CENTRCL=STLLIA(TM2,TH2,TCDB,AM,H,15,2)
IF (DUL.LT.0.0) CMLIC=-CMLIC
CMURC=STLLIA(TM2,TH2,TCDB,AM,H,15,2)
IF (CUR.GT.0.0) CMURC=-CMURC
CMLLC=STLLIA(TM2,TH2,TCDB,AM,H,15,2)
IF (CLL.LT.0.0) CMLLC=-CMLLC
CMLRC=STLLIA(TM2,TH2,TCDB,AM,H,15,2)
IF (CLR.GT.0.0) CMLRC=-CMLRC
FLUME EFFECTS
IF (AM.GE.1.6) GO TO 200
POK=F/1000
FM=2.1212E-06*HOK**3-5.2017E-04*HOK**2+.044193*HOK-9.0905E-04
DCMP=STLLIA(TM3,TETA2,TDCMP,AM,ETA,14,7)
IF (DCMP.LT.0.0) DCMP=0.0
LC2P=STLLIA(TM3,TETA2,TDC2P,AM,ETA,14,7)
IF (DC2P.GT.0.0) DC2P=0.0
DCMP=DC2P*FM
DCZF=STLLIA(TM3,TH1,TFMC,AM,H,14,3)
IF (FMC.GT.1.0) PMC=1.0
FNC=FM
PLD=STLLIA(TM3,TH1,TFMC,AM,H,14,3)
IF (FMC.GT.1.0) PLD=1.0
FQ=STLLIA(TM3,TH1,TFMC,AM,H,14,3)
IF (FQ.GT.1.0) PQ=1.0
FR=PC

```

```

C
PP=STGLIA(TM3,TH1,TFF,AM,H,14,3)
IF (PP.GT.1) EFFECTS
SEPARATESEP.LE.O) GC TC 200
IF (T.GE.1.0) GC TC 200
IF (T.GE.1.0) GC TC 200
FS2=(1.-ZTF/15.) *EXP(-ZTF/15.)
DCMSFF=CCLH(H,TH3,TECMSP,3)
DCZSFF=CCLH(H,TH3,TECZSP,3)
DCZSFF=FS2+ECZSPP
IF (ZTF.GE.4.0) GC TC 30
FS1=(1.-ZTF/4.) *EXP(-ZTF/4.)
DCVSFF=CCLH(H,TH3,TECYSP,3)
DCNSFF=ODLI(F,TH3,TECNSP,3)
DCVSFF=FS1+DCYSPP
DCNSFF=FS1+DCNSPP
CCLSF=-13*FS1
CPHI=CCS(FPI)
ECZSEP=ECZSP*CPHI+DCYSP*SPHI
DCYSEP=DCYSP*CPHI+DCNSP*SPHI
DCNSSEP=DCNSP*CPHI+DCMSF*SPHI
GO TO 100
TABLE CRUISE PHASE
ZERRC=LIFT DRAG
100 CCONTRC=STGLIA(TM2,TH2,TCC,AM,H,15,2)
CMULOC=STGLIA(TM4,TDCLT,TCMD2,AM,ADUL,5,4)
IF (CUL.LT.O) CMULC=-CMULOC
CMURC=STGLIA(TM4,TDCLT,TCMD2,AM,ADUR,5,4)
IF (CUR.GT.O) CMURC=-CMURC
CMLLC=STGLIA(TM4,TCCLT,TCMD2,AM,ADLL,5,4)
IF (CLL.LT.O) CMLLC=-CMLLC
CMLRC=STGLIA(TM4,TCCLT,TCMD2,AM,ADLR,5,4)
IF (CLR.GT.O) CMLRC=-CMLRC
CLC=CCLC+0017
ENCCF TAELE LCKK-UP
200 CMLLC=CALLC
CMURC=-CMURC
CMLLC=-CMLLC
CMURC=CMURC
CMURC=CMURC+DCZP
CMURC=CMURC+ECMP
CMURC=CMURC+CCSETA
TRANSFORM FROM CROSS-FLCW TO BODY AXIS COMPONENTS

```



```

SUBROUTINE A31
COMMON C(3415)
COMMON /FLAG/ FLG1
EQUIVALENCE (C(0601), FF1)
EQUIVALENCE (C(0602), WEIG)
EQUIVALENCE (C(0603), IA)
EQUIVALENCE (C(0604), FLG2)
FF1=C.C
WEIG=0.C
IA=0
FLG1=C.C
FLG2=C.C
RETURN
END

```

CC C C C C C C C

SUBROUTINE A3

THIS IS THE MISSILE PREPULSION MODULE

```

T1=BOOST ENGINE IGNITION TIME
BT=BOOST ENGINE BURNCUT TIME(=T3)
BE=CRUISE ENGINE IGNITION TIME(=T4)

```

```

COMMON /FLAG/ FLG1
COMMON C(3415)
EQUIVALENCE (C(0086), WEIGHT)
EQUIVALENCE (C(0110), T)
EQUIVALENCE (C(0932), T1)
EQUIVALENCE (C(0933), BT)
EQUIVALENCE (C(0935), BE)
EQUIVALENCE (C(0936), CG)
EQUIVALENCE (C(0136), CLT)
EQUIVALENCE (C(0150), CMT)
EQUIVALENCE (C(0151), CNT)
EQUIVALENCE (C(0152), EPSTH)
EQUIVALENCE (C(0153), PHITH)
EQUIVALENCE (C(0154), A)
EQUIVALENCE (C(0201), PC)
EQUIVALENCE (C(0202), TXEA)
EQUIVALENCE (C(0203), TYEA)
EQUIVALENCE (C(0074), TZE)
EQUIVALENCE (C(0075), F)
EQUIVALENCE (C(0507), AMACH)
EQUIVALENCE (C(0520), ETA)
EQUIVALENCE (C(0117), )

```



```

EQUIVALENCE (C(0601), FF1)
EQUIVALENCE (C(0602), WFIG)
EQUIVALENCE (C(0603), IA)
EQUIVALENCE (C(0604), FLG2)
EQUIVALENCE (C(0605), DIFFM)
EQUIVALENCE (C(0606), FLGRJ)
EQUIVALENCE (C(0508), CD)
EQUIVALENCE (C(2913), CEF)
DATA WFLLEL/189./

C 80 FORMAT(1H,10X,'TOTAL ANGLE OF ATTACK EXCEEDED, ETA=',F8.2)
C
IF (FLG1.GT.0.0) GO TO 1C
CT = 0.0
C DIFFM = C.0
FF = 0.0
TXBA = C.0
TYBA = C.0
TZBA = 0.0
IF (T.LI.11) RETURN
PIN = P*12.4.0254
TIN = T
AIN = ETA
IF (T.CE.BE) GO TO 1
C BCCST P-ASE
IT = T
IF (T.ET) GO TO 10
CALL BCCST (T, THRU, FF)
TXBA = T*RLS*COS(EPSTF)
TNEA = T*RLS*SIN(EPSTF)
TYBA = -TNEA*SIN(PHITF)
TZBA = TNEA*CCS(PHITF)
ID = 0
WEIGHT = WEIGHT-FF+FF1
CG = CG - (FF-FF1)/405.24
A = A - (FF-FF1)/256.25
B = B - (FF-FF1)/1.881
CC = B
CLT = C
CMT = TZBA*(15.525-CG)
CNT = -TYEA*(15.525-CG)
FF1 = FF
TW = T+DER
IF (T.LI.11) GO TO 2
IF (FLG2.GT.0.0) GO TO 2
WEIGHT = WEIGHT-31.
CG = CG -.15
FLG2 = 1.0

```

```

10 CONTINUE
   IF (FLGRJ.GT.0.0) GO TO 21
   CRUISE FFASE, RAMJET CFF
   IF (IB.GE.1) GO TO 11
   CALL ENGINE (PIN, AMACH, AIN, 0., TIN, 1.0, 0.0, 0., CT, SMARG, -1, 1)
   IB=1
11 IF (AIN.GT.9.3) AIN=9.3
   CALL ENGINE (HIN, AMACH, AIN, 0., TIN, 1.0, 0.0, 0., CT, SMARG, 1, 1)
   GO TO 4
C   SIMPLIFIED RAMJET MODEL
C   CRUISE FFASE, RAMJET CFF
21 CALL RAMJET (HIN, AMACH, AIN, FF, 1.0, CT)
   GO TO 4
1   CONTINUE
   IF (FLGRJ.GT.0.0) GO TO 22
   CRUISE FFASE, RAMJET CN
   IB=0
   IF (AIN.GT.10.0) GO TO 5
   FF=FF1
   IF (IA.GE.1) GO TO 3
   CALL ENGINE (HIN, AMACH, AIN, FF, TIN, 0.0, 0.0, 0.0, CT, SMARG, -1, 1)
   TT=1
   FF1=FF
   IA=1
   XIA=0
   IF (WEIG.GT.WFUEL) XIN=1.0
   CALL ENGINE (HIN, AMACH, AIN, FF, TIN, XIN, 0.0, 0.0, 0.0, CT, SMARG, 1, 1)
   GO TO 4
C   SIMPLIFIED RAMJET MODEL
C   CRUISE FFASE, RAMJET CN
22 IF (AIN.GT.10.0) GO TO 5
   XIN=0
   IF (WEIG.GT.WFUEL) XIN=1.0
   CALL RAMJET (HIN, AMACH, AIN, FF, XIN, CT)
   GO TO 4
5   IF (ELG1.GT.0.0) GO TO 10
   WRITE (C, 2) ETA
   GO TO 10
4   TXPA=CT*CD*S
   TYEA=0.
   TZBA=C
   CT=T-T1
   IF (FLGRJ.GT.0.0) GO TO 6
   FF=FF/.45359237
C   DIFFUSER (INLET) MARGIN IS NOT COMPUTED IN SIMPLIFIED RAMJET MODEL
   DIFFN=SMARG/100.

```

```

6  WFIG=WEIG+(ABS(FF+FF1))*CT/2.0
  IF (WEIG.GT.WFUEL) FLG1=1.0
  WEIGHT = WEIGHT - ABS(FF + FF1)*DT/2.
  TT=T
  FFI = FF
  CG=CG-.0026455*ABS(FF+FF1)*DT/2.
  A=A-.0031746*ABS(FF+FF1)*DT/2.
  B=B-.003452*ABS(FF+FF1)*DT/2.
  CC = B
  RETURN
2  ENC

```

CCU CCU

SUBROUTINE A4I ACTUATOR INITIALIZATION MODULE A4I

```

COMMON C(2415)
DIMENSION IPL(1071)
EQUIVALENCE (C(1735),WFIN)
EQUIVALENCE (C(3315),N)
EQUIVALENCE (C(3316),IPL(1))
IF (WFIN.GT.C.0) GO TO 100
GO TO 200
100 IPL(N+1)=1653
    IPL(N+2)=1657
    IPL(N+3)=1701
    IPL(N+4)=1705
    IPL(N+5)=1709
    IPL(N+6)=1713
    IPL(N+7)=1717
    IPL(N+8)=1721
    A=N+8
    RETURN
200 END

```

100

200

CCU CCU

SUBROUTINE A4 FIN ACTUATORS MODULE A4

```

COMMON C(2415)
EQUIVALENCE (C(1016),CPI)
EQUIVALENCE (C(1020),CC)
EQUIVALENCE (C(1024),DRI)
EQUIVALENCE (C(1693),CULC)

```



```

IF (ABS(C2).GE.RTLM) GC TO 130
GO TC 140
13C PRCD2=C2D*C2
IF (FRCD2.GE.0.0) C2D=0.0
C 140 LOWER=LEFT FIN RESPONSE
C3C=WFIN*(DLLC-CLL)-2.*DFIN*WFIN*D3
IF (ABS(C3).GE.RTLM) GC TC 150
GO TC 160
150 FRCC3=C3E*C3
IF (FRCC3.GE.0.0) C3E=0.0
C 160 LOWER=LEFT FIN RESPONSE
D4D=WFIN*(DLRC-CLR)-2.*DFIN*WFIN*D4
IF (ABS(C4).GE.RTLM) GC TO 170
GO TC 180
17C PRCD4=C4C*C4
IF (FRCD4.GE.0.0) C4C=0.0
18C GO TO 220
C *** IDEAL ACTUATORS ***
20C CUL=DULC
CUH=CULC
CLL=CLLC
CLR=DLFC
C FIN ANGLE LIMITERS
IF (ABS(CLL).GT.DMAX) CUL=SIGN(DMAX,DUL)
IF (ABS(CLR).GT.DMAX) CLR=SIGN(DMAX,CLR)
IF (ABS(CLL).GT.DMAX) CLL=SIGN(DMAX,DLL)
IF (ABS(CLR).GT.DMAX) CLR=SIGN(DMAX,CLR)
C PITCH YAW ROLL CHANNEL INPUTS
220 CQ=0.25*(CUL-CUR-CLR+CLL)
DR=0.25*(CUL+CUR-CLR+CLL)
CP=0.25*(CUL+CUR+CLR+CLL)
CULCEG=CUL*57.29578
RETURN
ENG
C
C SUBROUTINE A51
RETURN
END
C
C SUBROUTINE A5
RETURN
END

```

```

000 SUBROUTINE C11
000 INITIALIZATION MODULE FOR LVRJ AUTOPILOT
000
COMMON C(3415)
EQUIVALENCE (C(3315),N)
DIMENSION IPL(100)
IPL(N)=1677
IPL(N+1)=1689
IPL(N+2)=1725
IPL(N+3)=1725
N=N+4
RETURN
END

```

```

000 SUBROUTINE C1
000 SUBROUTINE C1-LVRJ
000 THIS AUTOFILCT MODULE IS FOR STV G
000
COMMON C(3415)
EQUIVALENCE (C(3315),N)
EQUIVALENCE (C(3316),IPL(1))
EQUIVALENCE (C(3317),IPL(2))
EQUIVALENCE (C(3318),IPL(3))
EQUIVALENCE (C(3319),IPL(4))
EQUIVALENCE (C(3320),IPL(5))
EQUIVALENCE (C(3321),IPL(6))
EQUIVALENCE (C(3322),IPL(7))
EQUIVALENCE (C(3323),IPL(8))
EQUIVALENCE (C(3324),IPL(9))
EQUIVALENCE (C(3325),IPL(10))
EQUIVALENCE (C(3326),IPL(11))
EQUIVALENCE (C(3327),IPL(12))
EQUIVALENCE (C(3328),IPL(13))
EQUIVALENCE (C(3329),IPL(14))
EQUIVALENCE (C(3330),IPL(15))
EQUIVALENCE (C(3331),IPL(16))
EQUIVALENCE (C(3332),IPL(17))
EQUIVALENCE (C(3333),IPL(18))
EQUIVALENCE (C(3334),IPL(19))
EQUIVALENCE (C(3335),IPL(20))
EQUIVALENCE (C(3336),IPL(21))
EQUIVALENCE (C(3337),IPL(22))
EQUIVALENCE (C(3338),IPL(23))
EQUIVALENCE (C(3339),IPL(24))
EQUIVALENCE (C(3340),IPL(25))
EQUIVALENCE (C(3341),IPL(26))
EQUIVALENCE (C(3342),IPL(27))
EQUIVALENCE (C(3343),IPL(28))
EQUIVALENCE (C(3344),IPL(29))
EQUIVALENCE (C(3345),IPL(30))
EQUIVALENCE (C(3346),IPL(31))
EQUIVALENCE (C(3347),IPL(32))
EQUIVALENCE (C(3348),IPL(33))
EQUIVALENCE (C(3349),IPL(34))
EQUIVALENCE (C(3350),IPL(35))
EQUIVALENCE (C(3351),IPL(36))
EQUIVALENCE (C(3352),IPL(37))
EQUIVALENCE (C(3353),IPL(38))
EQUIVALENCE (C(3354),IPL(39))
EQUIVALENCE (C(3355),IPL(40))
EQUIVALENCE (C(3356),IPL(41))
EQUIVALENCE (C(3357),IPL(42))
EQUIVALENCE (C(3358),IPL(43))
EQUIVALENCE (C(3359),IPL(44))
EQUIVALENCE (C(3360),IPL(45))
EQUIVALENCE (C(3361),IPL(46))
EQUIVALENCE (C(3362),IPL(47))
EQUIVALENCE (C(3363),IPL(48))
EQUIVALENCE (C(3364),IPL(49))
EQUIVALENCE (C(3365),IPL(50))
EQUIVALENCE (C(3366),IPL(51))
EQUIVALENCE (C(3367),IPL(52))
EQUIVALENCE (C(3368),IPL(53))
EQUIVALENCE (C(3369),IPL(54))
EQUIVALENCE (C(3370),IPL(55))
EQUIVALENCE (C(3371),IPL(56))
EQUIVALENCE (C(3372),IPL(57))
EQUIVALENCE (C(3373),IPL(58))
EQUIVALENCE (C(3374),IPL(59))
EQUIVALENCE (C(3375),IPL(60))
EQUIVALENCE (C(3376),IPL(61))
EQUIVALENCE (C(3377),IPL(62))
EQUIVALENCE (C(3378),IPL(63))
EQUIVALENCE (C(3379),IPL(64))
EQUIVALENCE (C(3380),IPL(65))
EQUIVALENCE (C(3381),IPL(66))
EQUIVALENCE (C(3382),IPL(67))
EQUIVALENCE (C(3383),IPL(68))
EQUIVALENCE (C(3384),IPL(69))
EQUIVALENCE (C(3385),IPL(70))
EQUIVALENCE (C(3386),IPL(71))
EQUIVALENCE (C(3387),IPL(72))
EQUIVALENCE (C(3388),IPL(73))
EQUIVALENCE (C(3389),IPL(74))
EQUIVALENCE (C(3390),IPL(75))
EQUIVALENCE (C(3391),IPL(76))
EQUIVALENCE (C(3392),IPL(77))
EQUIVALENCE (C(3393),IPL(78))
EQUIVALENCE (C(3394),IPL(79))
EQUIVALENCE (C(3395),IPL(80))
EQUIVALENCE (C(3396),IPL(81))
EQUIVALENCE (C(3397),IPL(82))
EQUIVALENCE (C(3398),IPL(83))
EQUIVALENCE (C(3399),IPL(84))
EQUIVALENCE (C(3400),IPL(85))
EQUIVALENCE (C(3401),IPL(86))
EQUIVALENCE (C(3402),IPL(87))
EQUIVALENCE (C(3403),IPL(88))
EQUIVALENCE (C(3404),IPL(89))
EQUIVALENCE (C(3405),IPL(90))
EQUIVALENCE (C(3406),IPL(91))
EQUIVALENCE (C(3407),IPL(92))
EQUIVALENCE (C(3408),IPL(93))
EQUIVALENCE (C(3409),IPL(94))
EQUIVALENCE (C(3410),IPL(95))
EQUIVALENCE (C(3411),IPL(96))
EQUIVALENCE (C(3412),IPL(97))
EQUIVALENCE (C(3413),IPL(98))
EQUIVALENCE (C(3414),IPL(99))
EQUIVALENCE (C(3415),IPL(100))

```



```

S2=0.0
AKCI=AKCI1
AKFI=AKFI1
AKPI=AKPI1
GO TC 16
C CRUISE ALTICFILCT
1 CONTINUE
S1=0.0
S2=1.0
AKCI=AKCI2
AKFI=AKFI2
AKPI=AKPI2
16 CONTINUE
C FITCH AND YAW CHANNELS
GI=AKG*(CN-S1*QC)
RI=AKR*RN
ANZM=-A2M/G
ANYM=AYM/G
ANZ=ANZC-ANZM
ANY=ANYC-ANYM
POS DCC AND DRC COMMAND NEG TURNING MOMENTS
DCCI=GI-S2*AKNZ*ANZ
ZID=CCC1
IF (ABS(CCC1-GE.DMAX) ZID=0.0
LQC=CCC1+AKCI*Z1
IF (ABS(LQC).GF.DMAX) DCC=SIGN(DMAX,DQC)
CRCI=RI-S2*AKNY*ANY
YID=CRCI
IF (ABS(CRCI-GE.DMAX) YID=0.0
LRC=CRCI+AKRI*Y1
IF (ABS(LRC).GF.DMAX) DRC=SIGN(DMAX,DRC)
2 CONTINUE
C ROLL CHANNEL
PLD=AKFI*FN
LAG CCPENSATOR
CMG1=.1
CMG2=.1
LPCD=-AKFI*(FN+P1)*QMG2/CMG1
LPCIC=(CMG1-CMG2)*CFCE-CMG2*DPCI
DPC=CFPCI+DFCD
IF (ABS(DPC).GE.DMAX) DPC=SIGN(DMAX,DPC)
RETURN
END
C C C
SUBROUTINE C21
C

```



```

DIMFASICA IPL(100)
COMMON C(3415)
EQUIVALENCE (C(0507),F)
EQUIVALENCE (C(3315),N)
EQUIVALENCE (C(3316),IPL(1))
IPL(N)=1633
IPL(N+1)=1637
N=N+2
HNCK=H
RETURN
END

```

CC C

SUERCLTINE C2
GLIDANCE CCMAND MODULE

```

COMMON C(3415)
EQUIVALENCE (C(0256),A33)
EQUIVALENCE (C(0286),VXTP)
EQUIVALENCE (C(0294),VYTP)
EQUIVALENCE (C(0302),VZTP)
EQUIVALENCE (C(0337),CMGYC)
EQUIVALENCE (C(0338),CMGZC)
EQUIVALENCE (C(0317),FLGT)
EQUIVALENCE (C(0335),XMA)
EQUIVALENCE (C(0340),YMA)
EQUIVALENCE (C(0341),ZMA)
EQUIVALENCE (C(0520),AMACH)
EQUIVALENCE (C(0500),ACC)
EQUIVALENCE (C(0501),PEF)
EQUIVALENCE (C(0502),HD)
EQUIVALENCE (C(0507),F)
EQUIVALENCE (C(0508),CF)
EQUIVALENCE (C(0515),PSF)
EQUIVALENCE (C(0527),GAT)
EQUIVALENCE (C(0528),VT)
EQUIVALENCE (C(0531),VF)
EQUIVALENCE (C(0581),CYNPI)
EQUIVALENCE (C(0582),AKG)
EQUIVALENCE (C(0932),T)
EQUIVALENCE (C(0933),T1)
EQUIVALENCE (C(0933),T2)
EQUIVALENCE (C(0933),T3)
EQUIVALENCE (C(0937),T5)
EQUIVALENCE (C(0942),TLC)
EQUIVALENCE (C(0944),TLC)
EQUIVALENCE (C(0945),TLC)

```

```

EQUIVALENCE (C11633), ANZCD)
EQUIVALENCE (C11636), ANZCI)
EQUIVALENCE (C11637), ANYCD)
EQUIVALENCE (C11640), ANYC)
EQUIVALENCE (C11750), WFI)
DATA RCCN/36500./
CYNP=CC/144.
C ZERC MODE CONTROL SWITCHES
S4=0.0
S5=C.C
S6=0.0
S8=0.0
IF (T.GE.T3) GO TC 1
IF (A.ACF.GE.2.0) GC TC 1
GO TC 100
C ZERC TRAJECTRY
1 IF (T.GE.T5) GO TO 2
GO TC 100
C LEVEL FLIGHT
2 IF (T.GE.TCC) GO TO 5
S4=1.0
S5=1.0
GO TC 100
C DIVE CLIMB
5 IF (T.GE.TLC) GO TO 4
7 PDCL=HCC
S4=1.0
S5=1.0
S8=1.0
GO TC 100
C ALTITUDE TO HREF
4 FORI2=SCRT(XMA**2+YMA**2)
DI=1.575*VF+PCCN-PCRIZ
IF (DI.GE.C.C) GO TC 6
S4=1.0
S5=1.0
S6=1.0
GO TC 100
C CIVE
CIVE (XMA*VZTP)/(XMA*VXTP+ZMA*VZTP)
W3=(ZMA*V)TP-2900.*W3/32.172+A33
ANZCI=-2.
IF (FLGT.GT.0.0) GC TC 8
GO TC 100
C TERMINAL PCPING
TERMINAL PCPING
ANZCI=ANGC*VT*CMGYC/22.174
GO TC 100
C CONTINUE
100 CONTINUE

```

```

C **** VERTICAL CHANNEL ****
C FERR LIMITER
  FERR1=56*(1-FREF)
  FERR2=C.5*FERR1
  IF (ABS(FERR1).GT.8CC) HERR2=SIGN(400.,HERR1)
  ANZC1=.0233*(S8*HCCI-S4*(HD+HERR2))+S5*A33
C NZ LIMITER
  IF (ANZC1) 108,107,106
108 AZMAX=.35*(CYNP-5.714)
  IF (CYNP.LE.20.0) AZMAX=E.5*DYNP/30.
  AZMAX=AMIN1(AZMAX,12.0)
  IF (ABS(ANZC1).GE.AZMAX) ANZC1=SIGN(AZMAX,ANZC1)
C 107 CONTINUE
C **** LATERAL CHANNEL ****
  ANYC1=C
  IF (1.175) GO TO 210
  IF (FLEGT.GT.0.0) GC TC 200
  C CROSS-PRCCCT MIDCOURSE GUIDANCE
  CPROD=(YMA*VXTP-XMA*VYTP)/(XMA*VXTP+YMA*VYTP)
  ANYC1=2900.*CPROD/32.172
  GO TO 205
C 200 ANYC1=AKG*VT*GMGZC/32.172
  C NY LIMITER
  205 IF (ANYC1) 208,207,208
  208 AYPAX=E.C*(DYNP-11.25)/22.5
  IF (CYNP.LE.22.5) AYPAX=4.0*DYNP/22.5
  AYPAX=AMIN1(AYMAX,12.0)
  IF (ABS(ANYC1).GT.AYPAX) ANYC1=SIGN(AYMAX,ANYC1)
C 207 CONTINUE
  C LATERAL LIMITING
  DENOM=SCRT((AZMAX*ANYC1)**2+(AYMAX*ANZC1)**2)
  IF (DENOM.LE.0.0) GC TO 210
  AZL1=AZMAX*ANYC1/DENOM
  IF (ABS(ANZC1).GE.ABS(AZL1)) ANZC1=AZL1
  AYL1=AYMAX*ANYC1/DENOM
  IF (ABS(ANYC1).GE.ABS(AYL1)) ANYC1=AYL1
  C LATERAL COMMAND FILTER
  210 ANYC1=WF1*(ANYC1-ANYC)
  C VERTICAL COMMAND FILTER
  ANZC1=WF1*(ANZC1-ANZC)
  RETCFN
  END
C
C SUBROUTINE C31
  RETURN
  END

```

CC	SUBROUTINE C3 RETURN END
CC	SUBROUTINE C41 RETURN END
CC	SUBROUTINE C4 RETURN END
CC	SUBROUTINE C51 RETURN END
CC	SUBROUTINE C5 RETURN END
CC	SUBROUTINE C61 RETURN END
CC	SUBROUTINE C6 RETURN END
CC	SUBROUTINE C71 RETURN END
CC	SUBROUTINE C7 RETURN END
CC	SUBROUTINE C81

RETURN
END

CC

SUBRCUTINE C8
RETURN
END

CC

SUBRCUTINE C9
RETURN
END

CC

SUBRCUTINE C5
RETURN
END

CC

SUBRCUTINE C101
RETURN
END

CC

SUBRCUTINE C10
RETURN
END

CCC

SUBRCUTINE C11

TRANSLATIONAL DYNAMICS INITIALIZATION MODULE D1A8
FOR USE WITH MODULE C1A CR D1B

C11A003C
C11A001C
C11A0020

DIMENSION IPL (100)
COMMON C(2415)
EQUIVALENCE (C(3315), A,)
EQUIVALENCE (C(3316), IPL(1))
IPL(N) = 283
IPL(N+1) = 251
IPL(N+2) = 259
IPL(N+3) = 287
IPL(N+4) = 255
IPL(N+5) = 303
N = N+6
RETURN
END

C11A007C
C11A0040
C11A005C
C11A0100
C11A011C
C11A012C
C11A013C
C11A014C
C11A0150
C11A016C
C11A0170
C11A0200

[illegible]


```

CP = (FCLLO)
A1 = CP + CS*ST*SF
A12 = CP + SS*ST*SP
A21 = CP + SS*ST*SP
A22 = CP + SS*ST*SP
A31 = CP + SS*ST*SP
A32 = CP + SS*ST*SP
A33 = CP + SS*ST*SP
IPL(N+1) = 213
IPL(N+2) = 217
IPL(N+3) = 221
IPL(N+4) = 225
IPL(N+5) = 229
IPL(N+6) = 233
IPL(N+7) = 237
IPL(N+8) = 241
IPL(N+9) = 245
IPL(N+10) = 249
IPL(N+11) = 253
N = N + 1
RETURN
END

```

CCC CCC

SUBROUTINE D2

ROTATIONAL DYNAMICS MODULE D2PA- PRINCIPAL AXES

```

COMMON /APFLE/ TM1(7), TM2(15), TM3(14), TM4(5), TETA1(7), TETA2(7),
1 TETA3(6), TX1(12), TX2(10), TX3(5), TX4(3), TH1(3), TH2(2),
2 TCZBC(7,2), TCDC(15,2), TCAD2(15), TCNBC(7,10,6), TCMOI(15,4),
3 TCMB(15,2), TCMD(15,2), TDCMDA(15), TPCMD(14,3), TCMQ(15), TPQ(14,3),
4 TCMBBC(7,2), TCLO(14,3), TPLD(14,3), TPLP(14,3), TDCYSP(3),
5 TDCZSP(3), TDCNSP(3), TH3(3), TFEJ(12), TFEJ(13)
1 EQUIVALENCE(EN, EN)
2 EQUIVALENCE(EN, EN)
3 EQUIVALENCE(EN, EN)
4 EQUIVALENCE(EN, EN)
5 EQUIVALENCE(EN, EN)
6 EQUIVALENCE(EN, EN)
7 EQUIVALENCE(EN, EN)
8 EQUIVALENCE(EN, EN)
9 EQUIVALENCE(EN, EN)
10 EQUIVALENCE(EN, EN)
11 EQUIVALENCE(EN, EN)
12 EQUIVALENCE(EN, EN)
13 EQUIVALENCE(EN, EN)
14 EQUIVALENCE(EN, EN)
15 EQUIVALENCE(EN, EN)
16 EQUIVALENCE(EN, EN)
17 EQUIVALENCE(EN, EN)
18 EQUIVALENCE(EN, EN)
19 EQUIVALENCE(EN, EN)
20 EQUIVALENCE(EN, EN)
21 EQUIVALENCE(EN, EN)
22 EQUIVALENCE(EN, EN)
23 EQUIVALENCE(EN, EN)
24 EQUIVALENCE(EN, EN)
25 EQUIVALENCE(EN, EN)
26 EQUIVALENCE(EN, EN)
27 EQUIVALENCE(EN, EN)
28 EQUIVALENCE(EN, EN)
29 EQUIVALENCE(EN, EN)
30 EQUIVALENCE(EN, EN)
31 EQUIVALENCE(EN, EN)
32 EQUIVALENCE(EN, EN)
33 EQUIVALENCE(EN, EN)
34 EQUIVALENCE(EN, EN)
35 EQUIVALENCE(EN, EN)
36 EQUIVALENCE(EN, EN)
37 EQUIVALENCE(EN, EN)
38 EQUIVALENCE(EN, EN)
39 EQUIVALENCE(EN, EN)
40 EQUIVALENCE(EN, EN)
41 EQUIVALENCE(EN, EN)
42 EQUIVALENCE(EN, EN)
43 EQUIVALENCE(EN, EN)
44 EQUIVALENCE(EN, EN)
45 EQUIVALENCE(EN, EN)
46 EQUIVALENCE(EN, EN)
47 EQUIVALENCE(EN, EN)
48 EQUIVALENCE(EN, EN)
49 EQUIVALENCE(EN, EN)
50 EQUIVALENCE(EN, EN)
51 EQUIVALENCE(EN, EN)
52 EQUIVALENCE(EN, EN)
53 EQUIVALENCE(EN, EN)
54 EQUIVALENCE(EN, EN)
55 EQUIVALENCE(EN, EN)
56 EQUIVALENCE(EN, EN)
57 EQUIVALENCE(EN, EN)
58 EQUIVALENCE(EN, EN)
59 EQUIVALENCE(EN, EN)
60 EQUIVALENCE(EN, EN)
61 EQUIVALENCE(EN, EN)
62 EQUIVALENCE(EN, EN)
63 EQUIVALENCE(EN, EN)
64 EQUIVALENCE(EN, EN)
65 EQUIVALENCE(EN, EN)
66 EQUIVALENCE(EN, EN)
67 EQUIVALENCE(EN, EN)
68 EQUIVALENCE(EN, EN)
69 EQUIVALENCE(EN, EN)
70 EQUIVALENCE(EN, EN)
71 EQUIVALENCE(EN, EN)
72 EQUIVALENCE(EN, EN)
73 EQUIVALENCE(EN, EN)
74 EQUIVALENCE(EN, EN)
75 EQUIVALENCE(EN, EN)
76 EQUIVALENCE(EN, EN)
77 EQUIVALENCE(EN, EN)
78 EQUIVALENCE(EN, EN)
79 EQUIVALENCE(EN, EN)
80 EQUIVALENCE(EN, EN)
81 EQUIVALENCE(EN, EN)
82 EQUIVALENCE(EN, EN)
83 EQUIVALENCE(EN, EN)
84 EQUIVALENCE(EN, EN)
85 EQUIVALENCE(EN, EN)
86 EQUIVALENCE(EN, EN)
87 EQUIVALENCE(EN, EN)
88 EQUIVALENCE(EN, EN)
89 EQUIVALENCE(EN, EN)
90 EQUIVALENCE(EN, EN)
91 EQUIVALENCE(EN, EN)
92 EQUIVALENCE(EN, EN)
93 EQUIVALENCE(EN, EN)
94 EQUIVALENCE(EN, EN)
95 EQUIVALENCE(EN, EN)
96 EQUIVALENCE(EN, EN)
97 EQUIVALENCE(EN, EN)
98 EQUIVALENCE(EN, EN)
99 EQUIVALENCE(EN, EN)
100 EQUIVALENCE(EN, EN)

```



```

AD22=A32*PBA-A12*RRBA
AD21=A31*PBA-A11*RRBA
AD13=A33*PBA-A33*ORBA
AD12=A32*PBA-A32*ORBA
AD33=A13*PBA-A23*PBA
AD32=A12*PBA-A22*PBA
AD31=A11*PBA-A21*PBA
AD23=A33*PBA-A13*RRBA
RETURN
END

```

CC

```

SUBROUTINE D31
RETURN
END

```

CC

```

SUBROUTINE D3
RETURN
END

```

CC

```

SUBROUTINE D41
RETURN
END

```

CC

```

SUBROUTINE D4
RETURN
END

```

CC

```

SUBROUTINE D51
RETURN
END

```

CC

```

SUBROUTINE D5
RETURN
END

```

CCC

```

SUBROUTINE G11

```

CCC

GRAVITATIONAL AND CCFCILIS ACCELERATION INITIALIZATION MODULE G11C

CCPMCN (13415)

SUBROUTINE G1
GRAVITATIONAL AND CORIOLIS ACCELERATION MODULE G1C

SUBCUTANE

GRAVITATIONAL AND CIRCLIS ACCELERATION MODULE GIC

[illegible]


```

A22=E22
A23=E23
A32=E32
A33=E33
VELCCITY IN BODY AXES
UBA=A11*VATX+A12*VATY+A13*VATZ
VBA=A21*VATX+A22*VATY+A23*VATZ
WBA=A31*VATX+A32*VATY+A33*VATZ
WELCCITY IN STABILITY AXES
LSA=VBA
VSA=VBA
WSA=-STS*UBA+CTS*WBA
ANGLE LF ATTACK AND SIDESLIP
ASA = ATAN(WSA/USA)
BSA = ARCSIN(VSA/SQRT(USA*USA + VSA*VSA + WSA*WSA))
RETURN
ENC

```

```

SUBROUTINE G4I
RETURN
ENC

```

```

SUBROUTINE G4
RETURN
ENC

```

```

SUBROUTINE G5I

```

COORDINATE CCNVERSION INITIALIZATION MODULE

```

COMMON C(3415)
EQUIVALENCE(C(0557),CTPI11)
EQUIVALENCE(C(0558),CTPI12)
EQUIVALENCE(C(0559),CTPI13)
EQUIVALENCE(C(0560),CTPI21)
EQUIVALENCE(C(0561),CTPI22)
EQUIVALENCE(C(0562),CTPI23)
EQUIVALENCE(C(0563),CTPI31)
EQUIVALENCE(C(0564),CTPI32)
EQUIVALENCE(C(0565),CTPI33)
EQUIVALENCE(C(0566),CTPI1)
EQUIVALENCE(C(0576),ALZ)
EQUIVALENCE(C(0578),AZ)
AZ = A27.C1745329

```

T>Y0126C
 T>Y0127C
 T>Y0128C

129

```

200 PSISF=CAGZ-P*STHTS-R*CTHTS
130 THILIM=SIGN(GMBLIM,THTS)
140 PSILIM=SIGN(GMBLIM,PSIS)
150 IF IABS(THTS).GT.GMBLIM) THTSD=50.*(THILIM-THTS)
    IF IABS(PSIS).GT.GMBLIM) PSISD=50.*(PSILIM-PSIS)
    RETURN
    FORMAT (1H,10X,'END CF SEARCH,NO TARGET DETECTION')
    FORMAT (1H,10X,'SEEKER LCST TARGET,LOOK ANGLE=',F8.3)
    FORMAT (1H,10X,'STARTY SEARCH,ATIGS TGT RGE=',F10.3,3X,'T=',F8.3)
    END

```

CC C

SUBROUTINE S2I

```

COMMON C(3415)
EQUIVALENCE (C(03361),FLGD)
EQUIVALENCE (C(03477),FLGTS)
FLGD=C.C
FLGTS=C.C
RETURN
END

```

CC CC

SUBROUTINE S2

```

RADICMETER MODULE S2

COMMON C(3415)
EQUIVALENCE (C(01721),RTAQ2)
EQUIVALENCE (C(02241),A11)
EQUIVALENCE (C(02248),A12)
EQUIVALENCE (C(02322),A13)
EQUIVALENCE (C(02361),A21)
EQUIVALENCE (C(02441),A22)
EQUIVALENCE (C(02448),A23)
EQUIVALENCE (C(02522),A31)
EQUIVALENCE (C(02552),A32)
EQUIVALENCE (C(02773),A33)
EQUIVALENCE (C(02777),THTS)
EQUIVALENCE (C(02801),PSIS)
EQUIVALENCE (C(02901),ANGLT)
EQUIVALENCE (C(02908),XTP)
EQUIVALENCE (C(03001),YTP)
EQUIVALENCE (C(03111),ZTP)
EQUIVALENCE (C(03112),ZTTP)

```



```

      IN(THTS)
      CPST=CPSTIS
      B112=CPSTIS*CTHTS
      B112=-CPSTIS*STHTS
      B211=-CPSTIS*CTHTS
      B221=CPSTIS*STHTS
      B311=0
      B321=0
      RESOLVE TGT POSITION FROM BODY SYSTEM TO SEEKER AXES
      XOT=B111*YMT+B12*YMT+B13*ZMT
      YOT=B211*YMT+B22*YMT+B23*ZMT
      ZOT=B311*YMT+B32*YMT+B33*ZMT
      RXVT=SCRT((YCT**2+ZCT**2)**.5)
      RESOLVE AT TGT POSITION FROM BODY SYSTEM TO SEEKER AXES
      XCA=E111*XMA+B12*YMA+B13*ZMA
      YCA=E211*XMA+B22*YMA+B23*ZMA
      ZCA=E311*XMA+B32*YMA+B33*ZMA
      IF (FLGS.GT.0.0) GC TC 5
      FLG1=0
      GO TC 2
      5 ANGLT=ATAN(RYZT/XCT)
      IF (FLGTS.GT.0.0) GC TO 30
      BETA=EFFECTIVE SEARCH BEAM WIDTH (DEG)
      BTAC2=6.2-7.07E-09*SCRT(CMGC*RAD/20.)*RMA**2
      TEST FOR TARGET DETECTION
      IF (FLG1.GT.0.0) GO TC 10
      FLG1=SET WHEN TARGET ENTERS BEAM
      IF (ABS(ANGLT).LE.BTAC2) FLG1=1.0
      GO TC 20
      10 IF (FLGC.GE.1.0) GC TC 20
      TIME=1
      FLGC=SET WHEN TARGET LEAVES BEAM
      IF (ABS(ANGLT).GE.BTAC2) FLGC=1.0
      GO TC 20
      20 DETECTION TIME DECLARED 30 MSEC AFTER TGT LEAVES BEAM
      IF (TC.GE.C.03) GO TC 25
      GO TC 20
      25 IF (FLGTS.GE.1.0) GC TC 20
      WRITE(6,160) T
      FLGTS=1.0

```

```

C
30 GO TC 200
   IF (FLIGHT-LE-0.0) GC TC 200
   RADICMETER SIGNAL
   CHI1=2.0193*(2.*ANGLT/3.-1.0)
   CHI2=2.0193*(2.*ANGLT/3.+1.0)
   IF (CHI1-EC-0.0) GO TC 40
   ERSIG=(SIN(CHI1)/CHI1)**2-(SIN(CHI2)/CHI2)**2
   GO TC 50
40 ERSIG=1.0-(SIN(CHI2)/CHI2)**2
   ERSIG=ZERU IF SPEKER LCSES TPACK
50 IF (ANGLT-2.5) ERSIG=0.0
   RESCLVE INTC AZ,EL ERRCR SIGNALS (SMALL ANGLE APPROX)
   IF (RYZT-LE-0.0) GC TC 60
   ERSZ=ERSIG*YDT/RYZT
   ERSZ=ERSIG*(-ZDT)/RYZT
   GO TC 60
60 ERSZ=C.0
   ERSZ=C.0
200 RETURN
160 FORMAT (1F,10X,'END CF SEARCH,TARGET DETECTED.T=',F8.3)
END

C
SUBROUTINE S3I
RETURN
END

C
SUBROUTINE S3
RETURN
END

C
SUBROUTINE S4I
RETURN
END

C
SUBROUTINE S4
RETURN
END

C
SUBROUTINE S5I
RETURN
END

C

```



```

C      AZA=EA31*AX1+BA32*AY1+BA23*AZ1
ACCELEROMETER QUANT. STEP=.194 G
AQS=6.22176
ANSX=AXA/ACS
AXMA=ACS*INT(ANSX)
ANSY=AYA/ACS
AYMA=ACS*INT(ANSY)
ANSZ=AZA/ACS
AZMA=ACS*INT(ANSZ)
TRANSCFORMATION BACK TC ECDY AXES
AXM=BA11*AXMA+BA21*AYMA+BA31*AZMA
AYM=BA12*AXMA+BA22*AYMA+BA32*AZMA
AZM=BA13*AXMA+BA23*AYMA+BA33*AZMA
C      *** ICEAL CYRCS ***
20 CM=C
RM=R
FM=P
RETUFA
END

C      SUBROUTINE S6I
RETURN
END

C      SUBROUTINE S6
RETURN
END

C      SUBROUTINE S7I
RETURN
END

C      SUBROUTINE S7
RETURN
END

C      SUBROUTINE S8I
RETURN
END

C      SUBROUTINE S8
RETURN
END

```


4W(18)/401.847/,W(19)/404.344/,W(20)/406.206/,W(21)/407.368/,
5W(22)/408.356/,W(23)/409.175/,W(24)/409.883/,W(25)/410.296/

C

TIME=T1-T1
IF(TIME.CT.C.) GO TC 3

FF=0.0
THRUST=C.0

GO TC 4

3 GO 1 I = 2.25 GC TC 2

1 CONTINUE

2 AK=(TIME-T(I-1))/(T(I)-T(I-1))
THRUST=F(I-1)+(F(I)-F(I-1))*AK

FF=W(I-1)+(W(I)-W(I-1))*AK

PSF=2116.217*(1.C-(C.87534703E-06)*H)**5.25627005)

THRUST=THRUST+12116.2-PSF)*.715428

RETURN

4 END

SUPERUTINE RAMJET (PIN,XMIN,AIN,WFIN,XIN,CT)

SIMPLIFIED RAMJET MODEL

USES TABLE LOCK-UP FOR THRUST COEFF AND FUEL FLOW RATE

DIMENSION TM(16),TM(217),TH(4),TETA(5),TCF1(6,5,4),TCF2(7,5,4),

1TMF(6,5,4)

COMMON C(3415)

C DATA TM1/2.3,2.5,2.7,2.9,3.1,3.3/

C DATA TM2/C.5,1.0,1.5,2.0,2.5,3.0,3.3/

C DATA TH/500.,1300.,2000.,3000.,35000./

C DATA TETA/C.2.,4.,6.,8./

C DATA TCF1/ .3814,.2558,.2075,.1374,
A.0644,.0443,.3794,.2843,.2025,.1339,.0805,.0402, .3731,.2818,
B.1515,.1203,.0666,.0258,.3476,.2526,.1655,.1049,.0555,.0173,
C.3251,.2355,.1595,.1001,.0549,.0201,.4357,.3412,.2453,.1651,
D.1111,.0662,.4337,.0253,.2401,.1654,.1075,.0639,.4273,.3268,
E.2287,.1512,.0927,.0485,.4012,.2967,.2061,.1350,.0810,.0396,
F.3762,.2751,.1954,.1200,.0805,.0425,.4944,.3861,.2798,.1963,
G.1341,.0666,.4924,.3731,.2742,.1924,.1256,.0832,.4857,.3706,.2618,
H.1766,.1132,.0666,.4573,.3376,.237,.1588,.1003,.056,.4328,.3186,

I-2254..1535..0999..C55..6273..5139..3561..2997..2243..1661..2054,
 J-6225..5028..3911..2566..2202..1616..6175..4598..3801..2821..2054,
 K-1455..5531..4721..3588..2662..1936..1367..5708..4555..3484,
 L-2613..1932..1398/

C

DATA TCF2/ -5727 -3661 -4238, 5727, -3658, -4235, -2618, -2067,
 A-2615, -2074, -2051, -4233, -2623, -2065, -2069, -2085,
 B-2072, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 C-5725, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 D-4205, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 E-2055, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 F-2074, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 G-3619, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 H-2074, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 I-2041, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 J-5664, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 K-4154, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 L-2055, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 M-3556, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 N-2577, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 O-2589, -2069, -3655, -4233, -2623, -2065, -2069, -2085,
 P-2017, -2069, -3655, -4233, -2623, -2065, -2069, -2085,

C

DATA TWF / 2.55, 2.95, 2.88, 2.85, 2.83, 2.85, 2.83, 2.85, 2.83,
 A2-806, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 B2-775, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 C2-604, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 D2-876, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 E2-812, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 F2-775, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 G2-812, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 H2-876, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 I2-812, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 J2-876, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,
 K2-812, 2.70, 2.65, 2.60, 2.55, 2.50, 2.45, 2.40, 2.35, 2.30,

C

I=FIN#3.280839895
 IF (X)IA.GT.0.0) GO TC 10
 RAMJET=CN CRUISE
 CT=THPRECL(XMIN,AIN,H,TM1,TETA,TH,TCF1,6,5,4)
 WFIN=0.0
 GO TC 20
 RAMJET=CN CRUISE
 CT=THPRECL(XMIN,AIN,H,TM2,TETA,TH,TCF2,7,5,4)
 WFIN=0.0
 RETURN
 2C END

C

```

SUBROUTINE ENGINE (PIN,XPIN,AIN,WFIN,TIN,XIN,YIN,ZIN,CT,SMARG,
1 IF1,IFRAD)
NWC COMMON DECK FOR AIRFREATHING PROPLUSICA PROGRAMS
CPIA ACNENCLATURE
REAL ISF,ISTAR,M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
REAL MACR,MACRS,MACF
INTEGER CCUNT
COMMON/CRUS/ ENG(30),IENG(15)
COMMON /RJ/ A,AINF,A1,A2,A3,A4,A5,A6,AR,AFR,AFS,ALPHA
COMMON /RJ/ ACR,BLEEC
COMMON /RJ/ CCASUB,CCASUP,COB,CF,CFINF,CF6,CF8,CFT,CFC,CNM
COMMON /RJ/ ER,ERRL,ETAC,ETAN,F
COMMON /RJ/ FAR,G,GAMMA,GAMMA1,GAMMA2,GAMMA3,GAMMA4,GAMMA5,GAMMA6
COMMON /RJ/ H,ISP,ISTAR,I1,I2,I3,I4,I5,I6,I7,I8,I9,I10
COMMON /RJ/ CCUNT,ICCNV,ICCNVP,IFIRST
COMMON /RJ/ MACR,MACRS,PM
COMMON /RJ/ P,P1,P2,P3,P4,P5,P6,PT301,PRAR
COMMON /RJ/ PT,PT1,PT2,PT3,PT4,PT5,PT6,PMOPT,PMOPT1,PMOPT2,PMOPT3
COMMON /RJ/ PH1,PH12,PH13,PH14,PH15,PH16,PTIPRI,Q
COMMON /RJ/ RADEG,R,SA,SARI,SQPTNT
COMMON /RJ/ T,T1,T2,T3,T4,T5,T6,TIME
COMMON /RJ/ TT,TT1,TT2,TT3,TT4,TT5,TT6
COMMON /RJ/ V,V1,V2,V3,V4,V5,V6
COMMON /RJ/ WA,WFX,X,Y,Z
* * * * *
COMMON /EXFALS/ TABLE(1000)
COMMON /WFITCT/ WRIT(20)
NAMELIST /MCNT/ ENG,IENG
** THE INFORMATION BELOW NOTES HOW THE NAMELIST
DATA IS INPUT AND WHAT THE INPUTS ARE **
ENG(1)=A1/AR OR A1 (M SC) SEE 16
ENG(2)=A3/AR CR A3 (M SC) SEE 16
ENG(3)=A4/AR CR A4 (M SC) SEE 16
ENG(4)=A5/AR OR A5 (M SC) SEE 16

```



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CCCCCCCCCCCC
ENG(1)=A6/AR CR A6 (N SC) SEE 16
ENG(6)=AR (METRES SQUARED) EFFICIENT
ENG(7)=CCE BURNER CARG COEFFICIENT
ENG(8)=ETAN NOZZLE THRUST EFFICIENCY
ENG(9)=ETAC COMBUSTION RATE (KG/SEC) SEE 15
ENG(10)=W5 STAR FLOW GAS GENERATOR SYSTEMS)
ENG(11)=152 CF PRIMARY GAS GENERATOR SYSTEMS)
ENG(12)=152 CF FLOW PERCENTAGE/100
ENG(13)=ELECT FUEL PERCENTAGE/100
ENG(14)=AIR FUEL RATIO
ENG(15)=CAN NOZZLE MASS FLOW COEFFICIENT

REAL MCCSE MCCSE(176), EAGLE(176)
DIMENSION MCCSE(176), EAGLE(176)

*** THE INPLTS BELOW ARE SWITCHES ***
IENG(1)=11, ENGINE TYPE SWITCH
IF I1=0, RAMJET TYPE IF I1=1, GAS GEN TYPE
IENG(2)=12, COMBUSTION EFF SWITCH
IF I2=0, ETAC IS SET BY INPUT
IF I2=1, ETAC IS SET IN A SUBROUTINE
IENG(3)=13, STANDARD DAY
I=2, 13, STANDARD DAY
IENG(4)=14, REAL AIR SWITCH SOLUTION
IF I4=0, USE THE GAMMA=1.4 SOLUTION
IF I4=1, USE THE GAMMA=1.4 SOLUTION
IENG(5)=15, USE ORCGRAM SWITCH IN THE SOLUTION
IF I5=1, THE PROGRAM USES WE IN THE SOLUTION
IF I5=2, 16, INLET CATS ARE ABSOLUTE VALUES
IENG(6)=16, THE INPLTS ARE ABSOLUTE VALUES
IF I6=0, DO NOT PRINT DEBUG DATA EACH ITERATION
IENG(7)=17, PRINT EACH ITERATION SWITCH
IF I7=0, DO NOT PRINT DEBUG DATA
IENG(8)=18, COMBUSTION PRESSURE EFFECT SWITCH
IF I8=0, THERE IS NO PRESSURE EFFECT COMPUTED
IF I8=1, THE PRESSURE EFFECT ON COMBUSTION TEMP IS COMPUTED

EQUIVALENCE(TABLE(206), MCCSE(1))
EQUIVALENCE(TABLE(382), EAGLE(1))

*** EXAMPLE OF NAMELIST INPUT ***
$MCNT
ENG=.5256,.05,.85,.44444,.56,.1140092,0,.98,.55,2,.50,1.2,.04,13.8
1.0,
IENG=C,0,2,C,1,0,0,0,
$END

```

```
C      IF (IREAL.EQ.1) GO TO 10
C      CMMENT=REAL IN DATA AND RETURN TO CALLING ROUTINE
C      CREAD(7,MCONT)
C      WRITE(6,MCONT)
C      RETURN
C      FLT DATA IN FORM THAT THE ATTODYC PROGRAM CAN USE
10    CCNTINLE
      PACCH=C.C
      P=XMIN
      ALPHA=AIRN
      WF=WFIJA
      TIME=TJJA
      IF(WFIA.LT.0.0001.AND.TIME.GT.20.) IFUEL=4
      IF(IPST.IFI)
        X=XIN          @ GAMMA
        Y=YIN          @ NOT USEC
        Z=ZIN          @ NOT USEC
      Z=ZINANG(11)
      A1=EANG(11)
      IF(TIME.GT.10.0) A1=.43244
      IF(TIME.GT.1C.O.AND.TIME.LT.50.0) A1=.43162+.00008639*TIME
      IF(TIME.GE.50.0) A1=.43294
      A3=EANG(3)
      A4=EANG(4)
      IF(XIN=O GE.1.C) IFUEL=5
      IF(TIME.LE.12.5) AS=.50226
      IF(TIME.GT.12.5.AND.TIME.LE.40.) AS=.51410+.00022839*TIME
      IF(TIME.GT.40..AND.TIME.LE.66.) AS=.51776+.00014694*TIME
      IF(TIME.GT.66.) AS=.52746
      A6=EANG(6)
      AR=EANG(7)
      CDPR=EANG(8)
      CTAN=EANG(9)
      ETAC(EANG(5).EQ.2) WF=EANG(10)
      IF(STAR=EANG(11))
      PHIE(EANG(12))
      PLFE(EANG(13))
      AFCS=EANG(14)
      CNM=EANG(15)
      IF(CAP.LT.0.5) CNM=1.0
      I1=EANG(11)
      I2=EANG(12)
```

```

13=IENG(2)
14=IENG(3)
15=IENG(4)
16=IENG(5)
17=IENG(6)
18=IENG(7)
IF (I6.EC.0) A1=A1*AR
IF (I6.EC.0) A3=A3*AR
IF (I6.EC.0) A4=A4*AF
IF (I6.EC.0) A5X=A5*AR
IF (I6.EC.0) A6=A6*AF
IF (I6.EC.1) A5X=A5
A5=A1X*CNM
IF (I6.EC.1) GC TC 20
GO TO INCL
CONTINUE
20 COMMENT INITIALIZE ,SET CONSTANTS AND WRITE AREAS
AIRREATHING GEOMETRY ONLY CALLED ON FIRST PASS
CALCULATE GEOMETRY PARAMETERS
A4OA5=A4/A5
GAM=5.0/7.0
M4=F*PARL(GAM,A4OA5)
PHI4=PPIM(GAM,M4)
A6CA5=A6/A5
M6=F*PARH(GAM,A6OA5)
PHI6=PPIM(GAM,M6)
IDENTIFY AND PRINT PARAMETERS
WRITE (6,420) A1
WRITE (6,440) A3
WRITE (6,450) A4
WRITE (6,460) A5X
WRITE (6,470) A6
WRITE (6,480) AR
WRITE (6,490) PHI4
WRITE (6,500) PHI6
WRITE (6,510) CDB
WRITE (6,520) CNM
CONTINUE
20 SET CCNANTS AND INITIALIZE SUBROUTINES
G IN KGM/SEC SQ - N

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```

C      RADEG=.572557779E+02
C      G=5.EC66E
C      START CALCULATIONS FOR EACH NEW POINT
C      COUNT=0
C      ICCNV=1
C      NEW ITERATIONS START HERE
C      4C ICCNV=C
C      CHECK TC SEE IF 100 ITERATIONS OF THE SAME PCINT HAVE BEEN MADE
C      IF (CCCNT-100) 60,60,50
C      IF NCT CCVERGED AFTER 100 ATTEMPTS, STOP
C      50 WRITE (6,530)
C      CALL EXIT
C      IF NCT CCVERGED WITH LESS THAN 100 ATTEMPTS, TRY AGAIN
C      6C CONTINUE
C      IF (CCCNT.GT.89) I7=1C
C      IF AECV STATEMENT NCT CCVERG,PRINT LAST 10
C      IF (COUNT.NE.0) GO TO 50
C      IF (IFIRST.EC.-1) CALL AIR(F,M,-1,P,T,A,DEN,Q,G,1,1)
C      IF (IFIRST.EC.-1) GC TC 70
C      I3=1E+10C
C      CALL AIR(F,M,1,P,T,A,DEN,Q,G,1,1)
C      G=5.EC66E
C      7C IF (I4.EC.1) GO TO EC
C      ENTPR IN CAL/GM
C      ENTHR=46.427E+.2394E+(T-194.444)
C      V IN METRES PER SEC
C      V=M*A
C      ENERG=(V**2.)/8368.
C      ENTHAL=ENTHR+ENERG
C      ECGP=ENTHAL+ENERG
C      ECGM IN CAL/GM
C      TT3 IN DEGREE RANKINE
C      TT3=539.31+(17.5164*E(CGM))-(3.3559E-03*ECGM*ECGM)+(4.65976E-06*(ECGP
C      1*#3.1))-(1.22556E-09*(ECGM**4.1))
C      TT=TT3/1.8
C      GAMMA3=1.4048-(6.09654E-04*ECGM)+(2.12102E-06*ECGM*ECGM)-(5.56845E

```

```

1-C5*(ECGM**3.))+(6.45543E-12*(ECGM**4.))
GO TC 130
EC CONTINUE
GAMMA3=1.4
TT3=TT/FT(TT(1.4,M))
T3=TT3*FT(TT(1.4,M3))
SC CONTINUE
C
IF (IFIRST) 100,11C,11C
100 WRITE (6,540)
C
COMBLSTC
C
IF (12:EC.1) CALL ETA
CALL TAE (AFS)
V=-0.0
WA=1C.C
M3=
MACRS=1.
CALL FCRA
C
CALCULATION
C
WRITE (6,230)
C
DIFFUSER
C
CALL HCF
GO TC 130
11C CONTINUE
IF (A.GT.1.07) GO TC 130
IF (AF.LT..001) GO TC 120
PT=P/FFFCPT(1.4,M)
PMOPT=FFFCPT(1.4,M)
TT=TT/FT(TT(1.4,M))
ACR=.27661+2.4721*M-4.527*M*M+2.3036*M*M*M
AINF=AINF*FT*PMOPT)/SCRT(TT)
WA=(AINF*FT*PMOPT)/SCRT(TT)
CALL HCRA
120 CONTINUE
IF (AF.LT..001) ER=0.0
FAR=ER/AFS
CALL SLESCN (M,M,FAR,CF,AF,Q,AR)
ICCNV=C
COUNT=C
GO TC 225
C ***** END OF SUBSCNIC CALL SEQUENCE *****

```

```

13C CONTINUE
C
C ***** WE SET SA HERE *****
IF (15.EC.1) GO TO 140
IF (15.EC.2) GO TO 150
WRITE (6,240)
C GC THIS ROUTE IF ER IS INPUT OR CHANGED IN HCRA
140 CONTINUE
CALL FCRA
IF (FUEL.EC.5) ER=0.0
FAR=ER/AFS
WF=FAR*WA
AFR=1./FAR
GO TO 16C
C GC THIS ROUTE IS WF IS INPUT OR SET IN HCRA
15C CONTINUE
CALL FCRA
IF (FUEL.EC.5) WF=0.0
FAR=WF/WA
ER=FAR*AFS
IF (FAR.EC.0.0) GO TO 1400
AFR=1./FAR
GO TO 16C
1400 AFR=0.0
C
C 16C CONTINUE
C
TOTTE=FTCTT(GAMMA3,M3)
T3=TT3+TCTT3
SORTCT=SCRT(TT3)
C
C TO FIND AIR SPECIFIC IMPULSE
C
IF (110.EC.0) GO TO 161
CONTINUE
GO TO 16C
161 CONTINUE
CALL INTR20 (TT3,ER,TT41,TABLE,1)
CALL INTR20 (TT3,ER,GAMMA4,TABLE,2)
CALL INTR20 (TT3,ER,MW4,TABLE,3)
C
C COMPUTE THE EFFECT OF PRESSURE ON TEMPERATURE
IF (18.EC.C) GO TO 162
G1=GAMMA4+1.C
G2=GAMMA4-1.0
G3=G1/G2

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1615 G4=2.*G1*(2./G1)**E3)
G5=SCRT(G4)
PT4=(S7*W4)/(G5*A5)
PT4ATM=PT4/101360.
IF(PT4ATM.LT.20.) PT4ATM=.20.
IF(PT4ATM.GT.20.) PT4ATM=20.
IF(TT3.LT.255.) GC TC 1615
IF(PT4ATM.GT.1.5) GO TO 1615
CTEMP=TC(TT3,SR,PT4ATM)
CONTINUE
TT4I=TT4I+CTEMP
162 CCNTINLE
C
C NEW FINISH CCMREUSTOR COMPUTATIONS
C
R=8214.24/MM4
WAX=W4/.45E5524
THROAT=AX/.C9290304
TTT=(TT3*1.8)/1000.)*2.
RSV=(W4)*TTT)/THROAT
IF(I2.EC.1) CALL ETA
TT4=ETAC*(TT4I+TT3)
BBB=2.*C*R*(1.0+GAMMA4)*TT4/GAMMA4
BBB=AMAX1(400.,BBB)
SA=(1.0+FAF)*SQRT(BEE)
SART=SA/SQRTCT
CCNTINLE
165
C
C COMMENT MAKE CALCULATIONS TAKING VARIABLE NOZZLE GAMMA INTO EFFECT
C
A4CA5=A4/A5
M4=FMARL(GAMMA4,A4CA5)
PT14=PT1M(GAMMA4,M4)
C
C ***** WE COMPUTE CONDITIONS AT STATION 3 HERE *****
C
STRCG=22.5613
IF(I1.EQ.1) GO TO 170
RANJET=CCFELTATIONS - FUEL ADDED IN THE INLETS
SART=STFCG*SQRT((GAMMA3+1.)/GAMMA3)*(1.+FAF)
PT13=(PT14*SART/SART)+(GAMMA3*CDB*M3*M3)/(2.*XMCIR3*SART))
GO TC 180
C
GAS GENERATOR SYSTEM COMPUTATIONS
SART=STFCG*SQRT((GAMMA3+1.)/GAMMA3)
PHI3=(PT14*SART/SART)-((PHIPRI*ISTAR*FAF)/(SART*SQRTGT))+(GAMMA
13*CCB*M3*M3)/(2.*XMCIR3*SART)
13*CCNTINLE
180 CCNTINLE
M3=FAFPHI(GAMMA3,PHI3)

```



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C 200 CONTINUE, INCREASE CCUNT AND CALCULATE PARAMETERS NOT IN COMMON
C SET IF15,
C COUNT=CCUNT+1
C CHECK CONVERGENCE, ICCNVF IS USED TO MAKE SOLUTION CONVERGE TWICE
C IF CCNVERGED, PRINT. IF NOT, GO BACK AND TRY AGAIN
C
C IF (IFIRST.EC.-1) GO TO 225
C IF (ICCNV+ICCNVP) 210,220,210
C 210 ICCNVF=ICCNV
C GO TO 40
C 220 CONTINUE
C ***** WE NOW COMPUTE THRUST IF CCNVERGED *****
C
C A6CA5=A6/A5
C M6=FMARH(GAMMA4,A6CA5)
C PH16=PT1M(GAMMA4,M6)
C IF(110.(E.5) GO TO 221
C CFC6=(MA*(SA*PH16*ETAN-A6*F))/(AR*Q)
C 221 CCNTINLE
C CCINF=2.*C*ACR*MACRS*A1/AR
C CALPHA=CCS(ALPHA/RACEG)
C CF=CF6-(CFINF*CALPHA)+CFB+CFC
C F=CF+C*AR
C IF(MF.EC.0.0) GO TO 1300
C ISF=F/(WF*G)
C GO TO 1500
C 1300 ISF=C.C
C 1500 CCNTINLE
C G1=GAMMA4+1.0
C G2=GAMMA4-1.0
C G3=G1/G2
C G4=2.*G1*(2./G1)**G3)
C G5=SCRT(G4)
C PTE=(SA*A)/(G5*A5)
C
C PREPARE DATA FOR TRANSFER TO MAIN PROGRAM
C
C 225 CONTINUE
C FIN=F
C XMIN=M
C AIN=ALPHA
C WFIA=WF
C CDADC=CCASUB+CDASUP+CFT
C CT=CF-CCACC

```

```

SMARG=FM ST ANT+.01
IF1=IF1RST ANT+.01
FCCUNT=CCFT=CI
WRIT(1)=AA
WRIT(2)=TT4
WRIT(3)=MACR
WRIT(4)=MACR
WRIT(5)=ER
WRIT(6)=ES
WRIT(7)=ES
WRIT(8)=ES
WRIT(9)=ETAC
WRIT(10)=ETAC
WRIT(11)=CT
WRIT(12)=FCCUNT
WRIT(13)=FCCUNT
WRIT(14)=ESV
WRIT(15)=EC.C.C) GO TC 120C
IF(PT3.EC.C.C)=PT5/PT3
CONTINUE
WRIT(16)=PT5/1000.
FCCUNT=FCCUNT
RETURN
120C

C
230 FORMAT (11F8.5)
240 FORMAT (12F8.5)
250 FORMAT (13F8.5)
260 FORMAT (14F8.5)
270 FORMAT (15F8.5)
280C
290C
300C
310C
320C
330C
340C
350C
360C
370C
380C
390C
400C
410C
420C
430C
440C
450C
460C

C
C COMPUTE PT13.1
C IS IS CUT (F RANGE-WHY.1)
C 11,F8.2,8F7.4,2F7.3,F7.2)
C 12F8.5)
C 13F8.5)
C 14F8.5)
C 15F8.5)
C 16F8.5)
C 17F8.5)
C 18F8.5)
C 19F8.5)
C 20F8.5)
C 21F8.5)
C 22F8.5)
C 23F8.5)
C 24F8.5)
C 25F8.5)
C 26F8.5)
C 27F8.5)
C 28F8.5)
C 29F8.5)
C 30F8.5)
C 31F8.5)
C 32F8.5)
C 33F8.5)
C 34F8.5)
C 35F8.5)
C 36F8.5)
C 37F8.5)
C 38F8.5)
C 39F8.5)
C 40F8.5)
C 41F8.5)
C 42F8.5)
C 43F8.5)
C 44F8.5)
C 45F8.5)
C 46F8.5)

C
C BREATHPING ENGINE GEOMETRY
C A 1 = F9.7,9H SQ METRE)
C A 2 = F9.7,9H SQ METRE)
C A 3 = F9.7,9H SQ METRE)
C A 4 = F9.7,9H SQ METRE)
C A 5 = F9.7,9H SQ METRE)

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470 FCFMAT (14H      A 6 = F9.7,9H SQ METRE)
480 FCFMAT (14H      A R = F9.7,9H SQ METRE)
490 FCFMAT (28H      F14 = F7.5)
500 FCFMAT (28H      F16 = F7.5)
510 FCFMAT (28H      BURNER DRAG COEFF. = F6.2)
520 FCFMAT (28H      NZZZLE MASS COEFF. = F6.2)
530 FCFMAT (36H      DID NOT CONVERGE AFTER 100 ATTEMPTS)
540 FCFMAT (14H      RAMJET PROPULSION
)

END

SUBROUTINE ETA

NWC COMPCN OFCK FCR AIRBREATHING PROPULSION PROGRAMS
CPIA NCMENCLATURE

REAL ISF,ISTAR,M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
REAL MACR,MACRS
INTEGER CCUNT

COMMON /RJ/ A,AINF,A1,A2,A3,A4,A5,A6,AR,AFR,AFS,ALPHA
COMMON /RJ/ ACR,BLFEEL
COMMON /RJ/ CDASUB,CDASUF,CDB,CF,CFINF,CF6,CFB,CFT,CFC,CNM
COMMON /RJ/ ER,ERRL,ETAC,ETAN,F
COMMON /RJ/ FAR,G,GAMMA,GAMMA1,GAMMA2,GAMMA3,GAMMA4,GAMMA5,GAMMA6
COMMON /RJ/ F,ISP,ISTAR,I1,I2,I3,I4,I5,I6,I7,I8,I9,I10
COMMON /RJ/ CCUNT,ICCNV,ICCNVP,IFIRST
COMMON /RJ/ M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
COMMON /RJ/ MACR,MACRS,PM
COMMON /RJ/ P,P1,P2,P3,P4,P5,P6,PT301,PRAR
COMMON /RJ/ PT,PT1,PT2,PT3,PT4,PT5,PT6,PMOFT,PMOFT1,PMOFT2,PMOFT3
COMMON /RJ/ PHI1,PHI2,PHI3,PHI4,PHI5,PHI6,PHI7,PHI8,PHI9,PHI10
COMMON /RJ/ RADEGR,RA,SA,SA1,SA2,SA3,SA4,SA5,SA6,SA7,SA8,SA9,SA10
COMMON /RJ/ T,T1,T2,T3,T4,T5,T6,TT1,TT2,TT3,TT4,TT5,TT6
COMMON /RJ/ V,V1,V2,V3,V4,V5,V6
COMMON /RJ/ WA,WB,X,Y,Z

DATA A11,E11,C11,D11,E11,F11,G11
* /-1407.66, -95416, -8.55033, 43.7266, 1468.91, 80484.,
* -277056./

FAR2=FAR*FAR
FOVER=1./((1.+FAR)

```

```

TERM1=P11+C11*FAR+D11*FAF2
TERM2=E11+F11*FAR+G11*FAR2
TTR=1.E+11
TT41=A11+TTR*TERM1+FCVER*TERM2
STT41=SCRT(TT41)
ETAC=40.246*STT41-0.2513*TT41-1055.08
ETAC=ETAC/1CC
IF(ETAC.LT. .0001) ETAC=0.0
RETURN
END

SUBROUTINE FCRA
DIMENSION FS(66), PSTAT1(11), FUELF(11)
NWC CCPMCA DECK FOR AIRBREATHING PROPULSION PROGRAMS
CPIA NCMENCLATURE
REAL ISP,ISTAR,M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
REAL MACR,MACRS
INTEGER CCLAT
CCPMCN /RJ/ A,AINF,A1,A2,A3,A4,A5,A6,AR,AFR,AFS,ALPHA
CCPMCN /RJ/ ACR,BLEEC
CCPMCN /RJ/ CDASUB,CDASUF,CDB,CF,CFINF,CF6,CF8,CFT,CFC,CNM
CCPMCN /RJ/ EF,EPFL,ERLL,ETAC,ETAN,F
CCPMCN /RJ/ FAR,G,GAMMA,GAMMA1,GAMMA2,GAMMA3,GAMMA4,GAMMA5,GAMMA6
CCPMCN /RJ/ F,ISP,ISTAR,I1,I2,I3,I4,I5,I6,I7,I8,I9,I10
CCPMCN /RJ/ CCUNT,ICCNV,ICCNVP,IFIRST
CCPMCN /RJ/ M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
CCPMCN /RJ/ MACR,MACRS,P4,P5,P6,PT301,PRAR
CCPMCN /RJ/ P1,P2,P3,P4,P5,P6,PT3,PT4,PT5,PT6,PMOPT,PMOPT1,PMOPT2,PMOPT3
CCPMCN /RJ/ PH1,PH2,PH3,PH4,PH5,PH6,PHI1,PHI2,PHI3,PHI4,PHI5,PHI6,PHI7,PHI8,PHI9,PHI10
CCPMCN /RJ/ RADEG,T1,T2,T3,T4,T5,T6,TIME
CCPMCN /RJ/ T1,T2,T3,T4,T5,T6,TT1,TT2,TT3,TT4,TT5,TT6
CCPMCN /RJ/ V,V1,V2,V3,V4,V5,V6
CCPMCN /RJ/ WA,WF,X,Y,Z
ANGLE CF ATTACK PS(1) I=3,14
PACH ALPHA PS(1) I=15,81
DATA PS/

```

CCCCC C CCCCCC C

CCCCC


```

C
C
A .5825,.5819,.5812,.5800,.5700,.5650,.5050,
A .6725,.6712,.6700,.6675,.6520,.6400,.6275,
A .5010,.5000,.4990,.4970,.4825,.4700,.4550,
A .5425,.5400,.5375,.5325,.5200,.5075,.4950,
A .5420,.5425,.9410,.5375,.9300,.9225,.9125,
A .5450,.5437,.9425,.5400,.9370,.9325,.9250,
A .5450,.5437,.9425,.5400,.9370,.9325,.9250/
C
C
C DATA XM/
A .5,.5,1,.1,4,1,6,2,2,2,4,3,2,4,8,2,5,2,7,3,0,3,25/
C
C DATA CALC/
A .0213,.0212,.0132,.125,.0988,.0221,.0184,.0173,.0171
B .0123,.0145,.0176/
C
C DATA B*P/
A .0339,.0239,.0208,.0237,.0249,.0334,.0287,.0265,.0259,
B .0213,.0171,.0150/
C
C IF (IFIRST) 10,20,20
10 CONTINUE
PRAR=0.0
TCL=.0004
WRITE (6,100) TCL
RETURN
C
C
C 20 CONTINUE
C
C SET PRESENT PR/AR EQUAL TC PREVIOUS PR/AR
PRAR=FFAF
C
C CALCULATE NEW PR/AR
C
TT=1/FTC(TT(1,4,M))
TT*ATC=SCRT(TT3/TT)
PRAR=TT*ATC*PMOPT*MACRS*AI/(PMOPT3*A2)
IF (IBC.EQ.0) PRAR=TT*ATC*PMOPT*MACRS*AI*(1.0+FAI)/(PMOPT3*A3)
C
C CHECK FOR CONVERGENCE BY COMPARING PR/AR TO PREVIOUS PR/AR
C
IF (ABS(PRAR-PRAR)-TCL) 40,40,30
30 ICNV=1
40 CONTINUE
C
C CALFA=CCS(ALPHA/RAI*EG)
C

```

```

C      COMPUTE CRITICAL PRESSURE RECOVERY AND MAXIMUM AIR CAPTURE RATIO
C
      ALPHA=AES(ALPHA)
      CALL INTR20 (M,ALPHA,PACR,AA,1)
      ELCT=CCL1(M,XM,BWR,12)
      BLEED=.015
      BLEED=ELCT*8LDD8
      MACRS=MACR*(1.0-BLEED)
      CALL INTR20 (M,ALPHA,FRIAD,PR,1)
      CRITICAL PRESSURE RECOVERY
      PACR=FRIAD
      IF (FRIAD-PACR) 50,60,70
      PRESSURE RECOVERY .LT. CRITICAL
50    FT301=FRAR
      ACR=1.
      GO TO 80
C
      PRESSURE RECOVERY .EQ. CRITICAL
60    PT301=FRIAD
      ACR=1.
      GO TO 80
C
      PRESSURE RECOVERY .GT. CRITICAL --CHANGE AIR CAPTURE AND SET PRES
      RECOVERY EQUAL TO CRITICAL VALUE
70    FT301=FRAR
      ACR=FRIAD/FRAR
      POPT=FFCPT(1.4,M)
      PT=PT/FCFT
      PT=PT*FT301
      PM=((FRIAD-PT301)/(FRIAD/100.))
      AINF=ACR*1*MACRS
      SQIAF=SQRT(TT)
      WA=(AINF*FT*FMOPT)/SQINF
      IF (ICGNVF.NE.0 .OR. ICCNV.EC.1) RETURN
      CDSUB=C.0
      IF (FRAR.LE.FACR) GC TC 50
C
      CALCULATE ADDITIVE CRAG CUE TO SUBSONIC SPILLAGE
      ETASUB=M/((M*10.2095)-11.5652)
      CDSUB=2.*(1.-ETASUB)*(1.-ACR)
C

```



```

C          CALCULATE ADDITIVE CDAG DUE TO SUPERSONIC SPILLAGE
90  CAEC=CL1(P,XM,CACC,12)
   IF (PRAR.LE.PACR) CDCLB=C.0
   CCASUB=CCSUB*AL/AR
   CCASCP=CAED
   CFB=C.C
C          CFT IS RAT DRAG
   CFT=C.CC/2
   PESI=2.14678-1.11435*M+.22989*M*M
   FE=PESI*F
   AINFB=A1*BLOCB
   AE=9.33*.00064516
   TRM1=P*AINFB*1.4*M*M
   TRM2=P*AE
   XDCT=((FT*AINFB*PMOPT))/SQTNF
   XME=XDCT*SCRT(TT-222.)/(PE*AE)
   XMC=FRCM(1.4,XMCE)
   TRM3=PE*AE*(1.+1.4*XME*XME)
   CFC=-((TRM1+TRM2-TRM3)/(C*AR))
   RETURN
C100  FORMAT (T6,'ALVRJ INLET DATA DEC 1975 ,TOL=',F7.6)
C          END
C          FUNCTION INTFP (AH,AL,BF,BL,FH,FM)
C          REAL INTFF
C2 = AL + (AH - AL)*FM
C1 = BL + (BF - BL)*FM
   INTFF = C1 + (C2 - C1)*FF
   RETURN
   END
C          FUNCTION FATAS(GAM,XM)
C          FUNCTION SUBPRCGFAM TO CALCULATE A OVER ASTAR
C          FRCF GAMPA AND NACT NUMBER
C          Z=(GAM+1.C)/(2.0*(GAM-1.C))
C          A=2.C/(GAM+1.0)
C          B=(GAM-1.0)/2.0
C          C=1.C/XM

```

FATA0030
 FATA001C
 FATA0020
 FATA004C
 FATA0050
 FATA0060
 FATA0070

FATA008C
FATA009C
FATA010C
FATA011C

R 2
R 4
R 6
R 8
R 10
R 12
R 14
R 16
R 18
R 20-

C=A*(1-C*(B**X**XM))
FATA=C*(C**Z)
RETURN
END

FUNCTION FIXAC (A)

TFIX=AES(A)-1.0000005
IF (TFIX.LT.0.0) GO TC 1C
IF (A.LT.0.0) GO TC 2C
FIXAC=C.C
GO TC 3C
20 FIXAC=1.14159265
3C CONTINUE
RETURN
END

CC C

S 2
S 4
S 6
S 8
S 10
S 12
S 14
S 16
S 18
S 20-

FUNCTION FIXAS (A)

TFIX=AES(A)-1.0000005
IF (TFIX.LT.0.0) GO TC 1C
IF (A.LT.0.0) GO TC 2C
FIXAS=1.57079633
GO TC 3C
20 FIXAS=-1.57079633
3C CONTINUE
RETURN
END

CC C

FAR0030
FAR001C
FAR002C
FAR004C
FAR005C
FAR006C
FAR007C
FAR008C
FAR009C
FAR010C
FAR011C

FUNCTION FMARH (GAM,ATAS)

FUNCTION SUBPROGRAM TO CALCULATE MACH NUMBER
FROM ATAS AND GAMMA

Z = (GAM + 1.0) / (2.0*(GAM - 1.0))
XMG = 10.0
XMG = 10.0
XMG = (XMG / 2.0
XMG = APX1(1.0,AMIN1(100.0,XMG))
IF (XMG - 1.000015)1C,1C,200
200 IF (CATAS = 1.0/XMG*(2.0*(GAM - 1.0) *XMG **2)/(GAM + 1.0))**Z
IF (CATAS - ATAS)700,100,800

CC C

FMAR0120
FMAR0130
FMAR0140
FMAR0150
FMAR0160
FMAR0170
FMAR0180

```

700 XMG = XPG + CXMG
    GO TO 500
800 XMG = XPG - DXMG
    GO TO 500
100 FMARL = XMG
    RETURN
    END

```

CCCC

```

FUNCTION FMARL(GAM,AR)
    FUNCTION ROUTINE TO FIND MACH FROM A/A* AND GAMMA
    USING NEWTON'S METHOD FOR FINDING ROOTS OF AN EQUATION
    SUBSCALIC SOLUTION
    IF(GAM.LT.1.) WRITE(6,20)
    IF(AR.LT.1.) WRITE(6,40)
    IF(GAM.LT.1. .OR. AR.LT.1.) CALL EXIT
    GM1=GAM-1.
    GPI=GAM+1.
    A=2./GFI
    B=GM1/(2.*GM1)
    Z=GFI/(2.*GM1)
    IF(AR.LT.1.3401) XMP=2.4706-(1.47059*AR)
    IF(AR.LT.1.34 .AND. AR.LT.3.001) XMP=.77443-(.2048*AR)
    IF(AR.GT.3.) XMP=(A**2)/AR
    TOL=.0001
    CCNT=1
    DO 10 INLE
    BRACK=A*(B*XMP*XMP)
    POWR=ERACK**Z
    TOF=(1./XMPF)-(AR/POWR)
    BOTTCM=(1./BRACK)-(1./XMPF*XMP)
    XM=XMP-(TCP/BOTTOM)
    CELTA=ABS(XM-XMP)
    XMP=XM
    IF(CELTA.GT.TOL) GO TO 10
    FMARL=XM
    RETURN
    FORMAT('GAMMA LT 1 IN FMARL')
    FORMAT('A/A* LT 1 IN FMARL')
    ENC

```

30
40
C
C
C
C
C

```

C      FUNCTION FPHIM (GAM , PHI )
C      CFMPHIM  FUNCTION SUBPRGAM TO CALC MACH NO  FROM PHIM
C
      TOL = .0001
      XMSN = 1.0 / ( PHI**2 )
      127 X = XMSN
      XMSN = (1.0 + (GAM*(XMSN**2))) / (PHI * SQRT(2.0 * (GAM+1.0))*(1.0
      1+(GAM-1.0)+.5*(XMSN**2)))
      XMSN = AMAX1(0. , AMIN1(1.0,XMSN))
      IF (ABS(X-XMSN)-TOL) 125, 128
      126 XMSN = (X + XMSN) / 2.0
      GO TO 127
      125 FMPHIM = XMSN
      RETURN
      END
C      FUNCTION FMPOPT (GAM,POPT)
C      CFMPOPT  FUNCTION SUBPRGAM TO CALC XMAC+
C      FROM P/PT ANC GAMMA
C
      Z = (FCPT) ** ((1.0-GAM)/GAM)
      SMPPT = (Z - 1.0)/(GAM - 1.0) * 2.0
      FMPCFT = SQRT(SMPPT)
      RETURN
      END
C      FUNCTION PHIM (GAM, XMCFT)
C      CPHIM  FUNCTION TO CALC PHI FROM GAMMA AND MACH
C
      PHIM = (1.0+GAM * (XMCFT**2)) / (XMCFT * SQRT(2.0*(GAM + 1.0)*(1.0+
      1.5*(GAM-1.0) * (XMCFT**2))))
      RETURN
      END
C      FUNCTION FPOPT (GAM,XPMACH)
C      CFPCPT  FUNCTION SUBPRGAM TO CALC TOTAL PRESSURE RATIO
C      FROM GAMMA ANC MACH NO.

```

FAPH0020

FAPH001C

FAPH003C

FAPH004C

FAPH005C

FAPH006C

FAPH007C

FAPH009C

FAPH010C

FAPH011C

FAPH012C

FAPH013C

FAPH014C

FAPH0030

FAPH001C

FAPH002C

FAPH004C

FAPH005C

FAPH006C

FAPH007C

FAPH008C

FPH002C

FPH001C

FPH003C

FPH004C

FPH005C

FPH006C

FPH003C

FPH001C

FPH002C

```

C      Z = -GAM / (GAM - 1.0)
C      FPOPT = (1.0+.5*(GAM - 1.0)*(XMACH**2))**Z
C      RETURN
C      ENC
C
C      FUNCTION FRCM(GAM,XMCIR)
C
C      FUNCTION ROUTINE TO COMPUTE MACH NUMBER FROM
C      MCIRCLE AND GAMMA FOR ALL MACH NUMBERS USING NEWTONS METHOD
C
C      IF (GAM.LT.1.) WRITE (6,100)
C      IF (GAM.LT.1.) CALL EXIT
C      A=GAM
C      P=0.5*(GAM*(GAM-1.))
C      C=XMCIR/.C5902063
C      XMP=C/(1.18+ (.0923*C))
C      TOL=.0001
C      1C CONTINUE
C      PRACK=A+(F*XMP*XMP)
C      PONE=SCFT(BRACK)
C      TOP=(XPF*FCWER)-C
C      BOTTLCH=(A+(2.*B*XMP*XMP))/POWER
C      XM=XPF-(TOP/BOTTLCH)
C      CELTA=ABS(XM-XMP)
C      XMF=XM
C
C      IF (DELTA.GT.TOL) GO TO 1C
C
C      FRCM=XM
C
C      RETURN
C
C      100 FORMAT('GAMMA LT 1 IN FROM')
C      END
C
C      FUNCTION FTCTT (GAM,XMACH)
C
C      FUNCTION SUBPROGRAM TO CALC T/TT FROM GAMMA AND MACH NC
C
C      FTOTTT = (1.0+.5*( GAM-1.0)*(XMACH**2))**(-1.0)
C      RETURN
C      END
C

```

```

CC C SUBROUTINE TAB(FAS)
C
C 15 WRITE(6,15)
FORMAT(16,'NO.2 JFS AND JETA FUEL MAY 1,1976 ONE ATM')
FAS= 14.6354
RETURN
END

CCC FUNCTION FMCIR (GAM,XM)
C
C MCIRCLE FUNCTION SUBPROGRAM TO CALC MCIR FROM GAMMA AND MACH NO
R AIR= 314.34/28.56246 = 287.073 N M/ KG K
M CIRCLE DIMENSION= SEC * SQRT(K) / METRE
FMCIR=.C55C2C6289*XM*SQRT(GAM*(1.0+((GAM-1.0)/2.0)*XM**2))
RETURN
END

CCC SUBROUTINE AIR (Z,V,J,P,T,S,D,Q,GO,K,KK)
C
C Z=ALTITUDE IN METERS
V=MACH NUMBER OR VELOCITY, SEE KK
J=FIRST PASS IDENTIFIER SWITCH, -=FIRST PASS AND +=NOT FIRST PASS
P=PRESSURE IN PASCALS OR PSI
T=TEMPERATURE IN K OR R
S=SPEED OF SOUND IN METERS/SEC OR FT/SEC
D=DENSITY IN KG/CUBIC METER OR LBM/CUBIC FT
GO=DYNAMIC PRESSURE IN PA OR PSI
KK=1, SI UNITS
KK=2, ENGLISH UNITS
KK=1, V IS VELOCITY, METERS/SEC OR FT/SEC
KK=2, V IS VELOCITY, METERS/SEC OR FT/SEC
DIMENSION A(2,16), C(15)
A(1,J),J=1,16
THESE ARE THE CHEBYSHEV COEFFICIENTS FOR P/PO
A(2,J),J=1,16
THESE ARE THE CHEBYSHEV COEFFICIENTS FOR D/DO

```

```

DATA A, Z10, -4.013517C, -2.2874890, -2.1765372,
A -4.0382210, -1.3585534, .0355105, .0458002,
B - .00552256, .0061561, .0030910, -.0121108,
C - .0026116, .0025277, .0004221, .0044268,
D - .0010261, .0039804, .0007523, -.0013126,
E - .00003145, .0033573, .0005513, -.0011477,
F - .0000031, .0021286, .0002918, .0008523,
H - .0001420, .0010109, .99998983, 1.0000000/

C ** SET CCNSTANTS
C
DATA PC, IC, RBAR, GC, Z1/
* 101225.0, 1.225, 287.07299, 9.80665, 30480.0/

C ** IF NECESSARY , CONVERT IC SI UNITS
C ** Z BECCMES METERS
C ** V BECCMES METERS/SEC
C
IF (K.EC.2) Z=Z*.3048
IF (K.EC.2.AND.KK.EC.2) V=V*.3048

C ** START HERE
C
IF (J) 10, 20, 20
1C WRITE (6,6C)
WRITE (6,7C) Z1

C ** CCMPUTE C(K) COEFFICIENTS
C
2C ETA=2.*(2.*Z/Z1-1.)
C(1)=ETA
C(2)=ETA**2-2.
DO 3C I=3,15
3C C(I)=ETA*C(I-1)-C(I-2)

C ** COMPLE CHEBYSHEV TRUNCATED EXPANSION
C
ALNP=1(1,1)
ALND=A(2,1)
DO 4C I=2,15
4C ALNF=ALNP+A(1,I)*C(I-1)
ALAC=ALND+A(2,I)*C(I-1)

C ** COMPLE ATMOSPHERIC PRESSURE
C ** P IN N/SQ METER
C
ALNF=.5*ALNF

```

```

CC FOFZ=EXP(ALNP)
CC F = FCFZ*FC*A(1,16)
CC
CC ** COMPUTE GRAVITY AT ALTITUDE AND LATITUDE
CC RC IS EQUATORIAL RADIUS (M) PER CRC HANDBOOK
CC GC IN M/SEC SQ
CC
CC FC=6376377.45
CC GO=GC*((RC/(RO+Z))**2)
CC
CC ** COMPUTE ATMOSPHERIC DENSITY
CC D IN KG PER CUBIC METRE
CC
CC ALND=.5*ALNC
CC DOZ=EXP(ALND)
CC L = CCLZ*CC*A(2,16)
CC
CC ** COMPUTE AIR TEMPERATURE
CC T IN DEGREE KELVIN
CC
CC T=P/(REAR*D)
CC
CC ** COMPUTE SPEED OF SOUND IN M/SEC
CC
CC S=SQRT(401.50219*T)
CC
CC ** COMPUTE DYNAMIC PRESSURE IN PA
CC
CC IF (KK.EC.1) Q=0.7*F*V**2
CC IF (KK.EC.2) Q=0.7*P*(V/S)**2
CC
CC ** CONVERT TO ENGLISH UNITS IF NECESSARY
CC
CC IF (K.EC.1) GC TO 50
CC Z=Z/.3048
CC IF (KK.EC.2) V=V/.3048
CC P=P/6894.757
CC T=T*1.8
CC S=S/.3048
CC C=C/16.01346
CC C=C/6894.757
CC GC=GC/.3048
CC RETURN
CC 50
CC 60 FORMAT (TS, '*** US 1962 STANDARD ATMOSPHERE')
CC 7C FORMAT (TS, '*** ALTITUDE FROM 0 TO ', F8.0, ' METERS.')
CC ENC

```

UU

UU


```

C
CC
CCC
FUNCTION ANORM(A,B)
CALCULATES TOTAL PRESSURE RATIO ACROSS A NORMAL SHOCK
A=GAMMA,E=XMACH
C=(A+1.)/2.
L=(A-1.)/2.
E=(L.*A)/(A+1.)
F=(A-1.)/(A+1.)
G=A/(A-1.)
F=1./(A-1.)
BB=B*B
ANUP=((C*E*F)/(1.+C*E*F))*G
LENU=((E*EE-F)**H)
ANCRP = ANUP/DEH
RETURN
END

```

```

END
      FUNCTION FPMOFT( GAM , XM )
      FUNCTION SUBPROGRAM TO CALCULATE P/PT * M CIRCLE
      FROM GAMMA AND MACH NUMBER
      DIMENSION S = SEC * SQRT(K) / METRE
      FPMOFT = FMCIR ( GAM , XM ) * FPOPT ( GAM , XM )
      RETURN
      END

```

```

SUBROUTINE SERCH (X,A,J,I,M)
  DIMENSION A(20)
  GO TO 1,I
  J=L
  IF (X.LE.A(L)) GO TO 20
  CONTINUE
  IF (J.EC.1) GO TO 30
  J=J-1
  RETURN
  10
  20
  30
END

```

```

C C C C C
FUNCTION SPECK(XM,C)
END

```

2 4 6 8 10 12 14 16 18 20
1111120

E 8888888888888888

```

C SHOCK FUNCTION SUBPROGRAM TO CALCULATE THE OBLIQUE SHOCK ANGLE FROM
C THE WEDGE ANGLE AND MACH NUMBER
C XM=MACH NUMBER C=WEDGE ANGLE DELTA IN RADIAN
C SHOCK=SHOCK ANGLE THETA IN RADIAN
C P,Q,R,A,B=CONSTANTS F=PHI WHICH IS AN INTERMEDIATE ANGLE
C RADEC=TRANSFORMS RADIAN TO DEGREE

```

```

RADEC = 57.2957795131
SINZCZ = SIN(C)
P = ((XM*XM+2.)/(XM*XM)) - (1.4*SINZCZ*SINZDZ)
CQ = 1.44 + (.4/(XM*XM))
C = ((2.*XM*XM)+1.)/(XM*XM*XM*XM)+(OQ*SINZDZ*SINZDZ)
R = (-C+((XM*XM*XM*XM)/C))
A = (1./3.)*((3.*Q-P*F)
B = (1./27.)*((2.*P*P*F-S.*F*Q +27.*R)
TEST = ((B*B)/4.)*((A*A)/27.)
IF (TEST) 1,1,2
1 CONTINUE
F = ARCCOS((-P/2.)/SCRT((-1./27.)*A*A*A))
FO = F*RADEC
FCX = (FC/3.)*240.
FCXE = FCX/RADEC
X = 2.*SCRT((-A/3.)*COS(FCXE)
SHOCK = ARSIN(SCRT(X-F/3.))
RETURN
WRITE(6,3)
3 FORMAT(48F) FCW COME THE INPUTS TO SHOCK GIVE COMPLEX ROOTS)
2 RETURN
END

```

```

2 4 6 8 10 12 14 16 18 20 22 24 26 28
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
C C C C C C C C C C C C C C C C

```

```

FUNCTION STOLI (TBX,TBY,TAB,X,Y,NX,NY)
FUNCTION DESIGNED TO ALLOW THE USER TO INPUT X
VARIABLE LENGTH TABLES. IT INTERPOLATES THE FIRST IN THE X
VARIABLE AND THEN IN THE Y VARIABLE. IT EXTRAPOLATES FROM
THE FIRST OR LAST INTERVAL IF THE X OR Y IS OUTSIDE OF THE
RANGES OF THE TABLE. IT REQUIRES THE SUBROUTINE SERCH FOR
ITS OPERATION.
FFGPRAMMER -- P.SOBEL 30 OCTOBER 1967
DIMENSION TBX(NX), TBY(NY), TAB(11,11)
CALL SERCH (X,TBX,I,NX,1)
CALL SERCH (Y,TBY,J,NY,1)
XX=TBX(I)

```

0246802446-
3313134444
0000000000

```

1C
      YV=TEY(J)
      TXY=TAE(I,J)
      XY=TAB(I,J)+(X-TBX(I))*((TAB(I+1,J)-TAB(I,J))/(TBX(I+1)-TBX(I)))
      XJ1=TAE(I,J+1)+(X-TBX(I))*((TAB(I+1,J+1)-TAB(I,J+1))/(TBX(I+1)-TBX(I)))
      STOL=XJ+(Y-TBY(J))*((XJ1-XJ)/(TBY(J+1)-TBY(J)))
      STCL=STCL
      FETUFA
      END

```

N 4000N4000N4000N400
111111NNNNNNNNNNNNNN

E EEEEEEEEEEENNEE EEEEEEEEEEE

```

FUNCTION STCLIA (TBX,TBY,TAB,X,Y,NX,NY)
      FUNCTION DESIGNED TO ALLOW THE USER TO INPUT
      VARIABLE LENGTH TABLES. IT INTERPOLATES FIRST IN THE X
      VARIABLE AND THEN IN THE Y VARIABLE. IT EXTRAPOLATES FROM
      THE FIRST OR LAST INTERVAL IF THE X OR Y IS OUTSIDE OF THE
      BOUNDS OF THE TABLE. IT REQUIRES THE SUBROUTINE SERCH FOR
      ITS OPERATION.
      FFCGRAMMER -- P.SOBEL 30 OCTOBER 1967
      DIMENSION TBX(NX), TBY(NY), TAB(NX,NY)
      CALL SERCH (X,TBX,I,NX,IC)
      CALL SERCH (Y,TBY,J,NY,JC)
      XJ=TAB(I,J)+(X-TBX(I))*((TAB(I+1,J)-TAB(I,J))/(TBX(I+1,J)-TBX(I)))
      XJ1=TBX(I,J+1)+(X-TBX(I))*((TAB(I+1,J+1)-TAB(I,J+1))/(TBX(I+1,J+1)-TBX(I)))
      STCL1=X+(Y-TBY(J))*((XJ1-XJ)/(TBY(J+1)-TBY(J)))
      STCLIA=STCL1
      RETURN
END

```

SUBRCUTINAE SUBSON(H, 2M, F, C, W, Q, A)

```

C=3
SFC= C4ECS* CQ* A
THR= :ZFC* IFR / 3600.
WF= W* F. 4. E= E
WIF(W. LT. 0.0) W=-W
ENCL

```

```

C
C      FUNCION  VECMAG(X)
C
      DIMENSION X(3)
      X2=X(1)*X(1)+X(2)*X(2)+X(3)*X(3)
      VECMAG=SQRT(X2)
      RETURN
      END

```

END

FUNCTION TC (T,FR,ATM)

THEORETICAL TEMPERATURE RISE CORRECTION FOR PRESSURES OTHER
THAN ONE ATMOSPHERE (HYDROCARBON FUELS)

DIMENSION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	52
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539214-0461127
CHECK FOR ENTRY OUTSIDE LATTICE

	IF	(T	LT	258.)	GO	TC	50
	IF	(T	GT	1300.)	GO	TC	60
	IF	(ER	GT	1.1.2)	GO	TC	70
	IF	(AT	LT	1.2)	GO	TC	50
	IF	(AT	LT	1.20.)	GO	TC	80

```

C
C IF (AIR.E1.E2.E3.E4.E5.E6.E7.E8.E9.E10.E11.E12.E13.E14.E15.E16.E17.E18.E19.E20.E21.E22.E23.E24.E25.E26.E27.E28.E29.E30.E31.E32.E33.E34.E35.E36.E37.E38.E39.E40.E41.E42.E43.E44.E45.E46.E47.E48.E49.E50.E51.E52.E53.E54.E55.E56.E57.E58.E59.E60.E61.E62.E63.E64.E65.E66.E67.E68.E69.E70.E71.E72.E73.E74.E75.E76.E77.E78.E79.E80.E81.E82.E83.E84.E85.E86.E87.E88.E89.E90.E91.E92.E93.E94.E95.E96.E97.E98.E99.E100.E101.E102.E103.E104.E105.E106.E107.E108.E109.E110.E111.E112.E113.E114.E115.E116.E117.E118.E119.E120.E121.E122.E123.E124.E125.E126.E127.E128.E129.E130.E131.E132.E133.E134.E135.E136.E137.E138.E139.E140.E141.E142.E143.E144.E145.E146.E147.E148.E149.E150.E151.E152.E153.E154.E155.E156.E157.E158.E159.E160.E161.E162.E163.E164.E165.E166.E167.E168.E169.E170.E171.E172.E173.E174.E175.E176.E177.E178.E179.E180.E181.E182.E183.E184.E185.E186.E187.E188.E189.E190.E191.E192.E193.E194.E195.E196.E197.E198.E199.E200.E201.E202.E203.E204.E205.E206.E207.E208.E209.E210.E211.E212.E213.E214.E215.E216.E217.E218.E219.E220.E221.E222.E223.E224.E225.E226.E227.E228.E229.E230.E231.E232.E233.E234.E235.E236.E237.E238.E239.E240.E241.E242.E243.E244.E245.E246.E247.E248.E249.E250.E251.E252.E253.E254.E255.E256.E257.E258.E259.E260.E261.E262.E263.E264.E265.E266.E267.E268.E269.E270.E271.E272.E273.E274.E275.E276.E277.E278.E279.E280.E281.E282.E283.E284.E285.E286.E287.E288.E289.E290.E291.E292.E293.E294.E295.E296.E297.E298.E299.E300.E301.E302.E303.E304.E305.E306.E307.E308.E309.E310.E311.E312.E313.E314.E315.E316.E317.E318.E319.E320.E321.E322.E323.E324.E325.E326.E327.E328.E329.E330.E331.E332.E333.E334.E335.E336.E337.E338.E339.E340.E341.E342.E343.E344.E345.E346.E347.E348.E349.E350.E351.E352.E353.E354.E355.E356.E357.E358.E359.E360.E361.E362.E363.E364.E365.E366.E367.E368.E369.E370.E371.E372.E373.E374.E375.E376.E377.E378.E379.E380.E381.E382.E383.E384.E385.E386.E387.E388.E389.E390.E391.E392.E393.E394.E395.E396.E397.E398.E399.E400.E401.E402.E403.E404.E405.E406.E407.E408.E409.E410.E411.E412.E413.E414.E415.E416.E417.E418.E419.E420.E421.E422.E423.E424.E425.E426.E427.E428.E429.E430.E431.E432.E433.E434.E435.E436.E437.E438.E439.E440.E441.E442.E443.E444.E445.E446.E447.E448.E449.E450.E451.E452.E453.E454.E455.E456.E457.E458.E459.E460.E461.E462.E463.E464.E465.E466.E467.E468.E469.E470.E471.E472.E473.E474.E475.E476.E477.E478.E479.E480.E481.E482.E483.E484.E485.E486.E487.E488.E489.E490.E491.E492.E493.E494.E495.E496.E497.E498.E499.E500.E501.E502.E503.E504.E505.E506.E507.E508.E509.E510.E511.E512.E513.E514.E515.E516.E517.E518.E519.E520.E521.E522.E523.E524.E525.E526.E527.E528.E529.E530.E531.E532.E533.E534.E535.E536.E537.E538.E539.E540.E541.E542.E543.E544.E545.E546.E547.E548.E549.E550.E551.E552.E553.E554.E555.E556.E557.E558.E559.E560.E561.E562.E563.E564.E565.E566.E567.E568.E569.E570.E571.E572.E573.E574.E575.E576.E577.E578.E579.E580.E581.E582.E583.E584.E585.E586.E587.E588.E589.E590.E591.E592.E593.E594.E595.E596.E597.E598.E599.E600.E601.E602.E603.E604.E605.E606.E607.E608.E609.E610.E611.E612.E613.E614.E615.E616.E617.E618.E619.E620.E621.E622.E623.E624.E625.E626.E627.E628.E629.E630.E631.E632.E633.E634.E635.E636.E637.E638.E639.E640.E641.E642.E643.E644.E645.E646.E647.E648.E649.E650.E651.E652.E653.E654.E655.E656.E657.E658.E659.E660.E661.E662.E663.E664.E665.E666.E667.E668.E669.E670.E671.E672.E673.E674.E675.E676.E677.E678.E679.E680.E681.E682.E683.E684.E685.E686.E687.E688.E689.E690.E691.E692.E693.E694.E695.E696.E697.E698.E699.E700.E701.E702.E703.E704.E705.E706.E707.E708.E709.E710.E711.E712.E713.E714.E715.E716.E717.E718.E719.E720.E721.E722.E723.E724.E725.E726.E727.E728.E729.E730.E731.E732.E733.E734.E735.E736.E737.E738.E739.E740.E741.E742.E743.E744.E745.E746.E747.E748.E749.E750.E751.E752.E753.E754.E755.E756.E757.E758.E759.E760.E761.E762.E763.E764.E765.E766.E767.E768.E769.E770.E771.E772.E773.E774.E775.E776.E777.E778.E779.E780.E781.E782.E783.E784.E785.E786.E787.E788.E789.E790.E791.E792.E793.E794.E795.E796.E797.E798.E799.E800.E801.E802.E803.E804.E805.E806.E807.E808.E809.E810.E811.E812.E813.E814.E815.E816.E817.E818.E819.E820.E821.E822.E823.E824.E825.E826.E827.E828.E829.E830.E831.E832.E833.E834.E835.E836.E837.E838.E839.E840.E841.E842.E843.E844.E845.E846.E847.E848.E849.E850.E851.E852.E853.E854.E855.E856.E857.E858.E859.E860.E861.E862.E863.E864.E865.E866.E867.E868.E869.E870.E871.E872.E873.E874.E875.E876.E877.E878.E879.E880.E881.E882.E883.E884.E885.E886.E887.E888.E889.E890.E891.E892.E893.E894.E895.E896.E897.E898.E899.E900.E901.E902.E903.E904.E905.E906.E907.E908.E909.E910.E911.E912.E913.E914.E915.E916.E917.E918.E919.E920.E921.E922.E923.E924.E925.E926.E927.E928.E929.E930.E931.E932.E933.E934.E935.E936.E937.E938.E939.E940.E941.E942.E943.E944.E945.E946.E947.E948.E949.E950.E951.E952.E953.E954.E955.E956.E957.E958.E959.E960.E961.E962.E963.E964.E965.E966.E967.E968.E969.E970.E971.E972.E973.E974.E975.E976.E977.E978.E979.E980.E981.E982.E983.E984.E985.E986.E987.E988.E989.E990.E991.E992.E993.E994.E995.E996.E997.E998.E999.E1000.E1001.E1002.E1003.E1004.E1005.E1006.E1007.E1008.E1009.E1010.E1011.E1012.E1013.E1014.E1015.E1016.E1017.E1018.E1019.E1020.E1021.E1022.E1023.E1024.E1025.E1026.E1027.E1028.E1029.E1030.E1031.E1032.E1033.E1034.E1035.E1036.E1037.E1038.E103
```

```

C      F1=-(.227276E-3+.100807E-6*T)*T+.018785)
      F2=1.0C12CG97-.1254E-5*T)*T+.0846043
      F3=1.0C113312E-7-.244175E-11*T)*T-.141615E-4)*T+.00496295)*T+.0056
      A0473
C
C      LINEARLY INTERPOLATE FOR FACTORS G1,G2,G3
      DO 10 I=1,3
      IF (ER.LE.E(I)) GO TO 20
      10 CCATINLE
      J=I-1
      R=(ER-E(J))/(E(I)-E(J))
      G1=G(J,1)+(G(I,1)-G(J,1))*R
      G2=G(J,2)+(G(I,2)-G(J,2))*R
      G3=G(J,3)+(G(I,3)-G(J,3))*R
C
C      LINEARLY INTERPOLATE FOR FACTORS H1,H2
      DO 30 I=1,13
      IF (ATM.LE.P(I)) GO TO 40
      30 CCATINLE
      J=I-1
      R=(ATM-P(J))/(P(I)-P(J))
      H1=H(J,1)+(H(I,1)-H(J,1))*R
      H2=H(J,2)+(H(I,2)-H(J,2))*R
C
C      COMPLETE TEMPERATURE CORRECTION (TC)
      TC=C(1)*F1*G1*H1+C(2)*F2*G2*H1+C(3)*F1*G2*H2+C(4)*F2*G1*H2
      D=C(5)*F3*G3*H1
      E=C(6)*F2*G3*H2
      F=C(7)*F3*G2*H2
      G=C(8)*F1*G3*H2
C
      RETURN (C,110)
50 GO TO 100
60 WRITE (C,120)
70 GO TO 100
80 WRITE (C,130)
90 GO TO 100
100 WRITE (C,150)
110 GO TO 100
120 WRITE (C,140)
130 CALL EXIT
140 RETURN
C

```



```

CC 1C 11=4,IX1
IF(I)
  IF(X,LT,C(I)) GO TO 11
  CONTINUE
10 IO=1-1
  IX2=IX1+4
  IX3=IX1+N2
  DO 2C JC=IX2,IX3
  J=JJ
  IF(Y,LT,C(J)) GO TO 21
  CONTINUE
20 JO=J-IX1
  NA=1+3+N2*((L-1)*N1+IC-2)+JO-1
  F1=(X-C(I-1))/(O(I)-C(I-1))
  F2=(Y-C(J-1))/(O(J)-C(J-1))
  F3=F1+F2
  C= C(NA)*((1,-F1-F2+F3)
  1 + C(NA+N2)*(F1-F3)
  2 + C(NA+1)*(F2-F3)
  3 + C(NA+N2+1)*F3
  RETURN
END

```

CCC CCCC

FUNCTION TPREOL (X,Y,Z,AX,AY,AZ,XYZ,NX,NY,NZ)

THIS FUNCTION INTERPOLATES LINEARLY IN THREE DIMENSIONS. IT
 SELECTS THE TWO PLANES OF CONSTANT Z AND USES STDLI FOR TWO DIMEN-
 SIONAL INTERPOLATION. A LINEAR INTERPOLATION IS USED IN Z.
 PFCG FROM H. SOBEL DATE 22 AUGUST 1968
 DIMENSION AX(NX), AY(NY), AZ(NZ), XYZ(NX,NY,NZ)
 DATA N1,1/
 CALL SEFCT (Z,AZ,K,NZ,M)
 AL=STDLIA(AX,AY,XYZ(1,1,K),X,Y,NX,NY)
 AU=STDLIA(AX,AY,XYZ(1,1,K+1),X,Y,NX,NY)
 THREECL=AL+(AU-AL)*(Z-AZ(K))/(AZ(K+1)-AZ(K))
 RETURN
 END

2 4 6 8 10 12 14 16 18 20 22 24 26-
 F F F F F F F F F F F F F F F

LIST OF REFERENCES

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